

Lecture #4

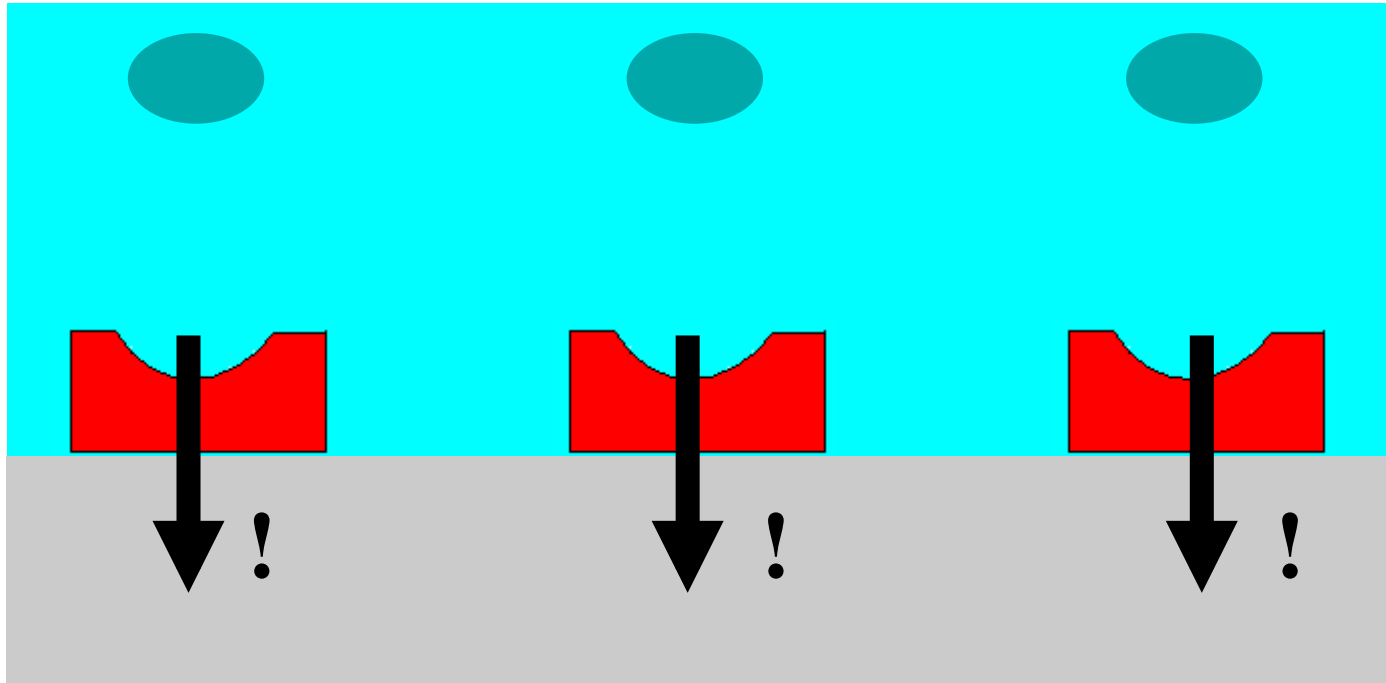
Probe Detection Principles (Faradaic Processes)

Lecture Outline

(Book Bio/CMOS: Chapter' paragraphs § 8.2 & 8.5-8)

- Electrochemical interfaces with enzymes
- Faradaic currents at the interface
- Electrochemical cells and equivalent circuits
- Calibration curve, Sensitivity, and LOD

CMOS/Sample interface



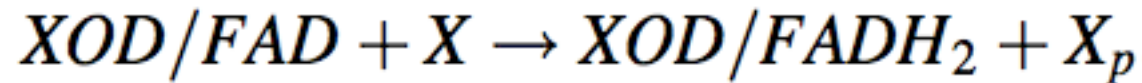
We may exploit some catalyzed reactions with transfer of electrons for detection aims at our Bio/CMOS interfaces

Enzymes' based detection

In the case of some enzymes, we can easily exploit the redox reactions involving their substrates to the aim of electrochemical direct detection: e.g., that's the case of oxidases and cytochromes.

Redox with oxidases

The typical redox involving an oxidase is as follows:

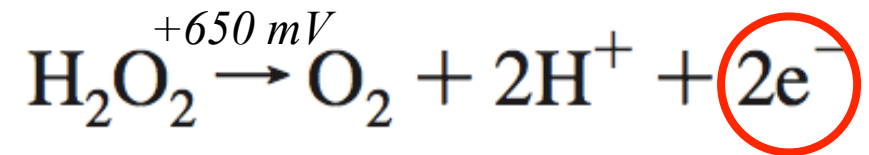


The FAD (Flavin Adenine Dinucleotide) is a functional part of the protein that gains a hydrogen molecule after the reaction. Therefore, the oxidase is not yet ready for another transformation because the FAD has gained the H_2 . To return to its initial state, the enzyme needs to release that hydrogen molecule:

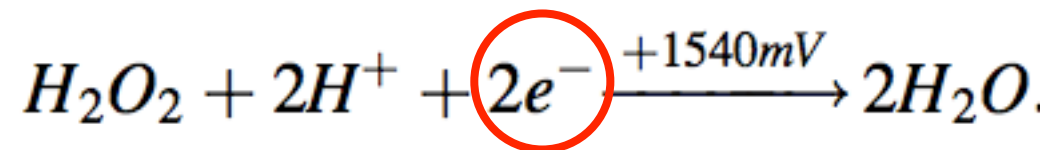


Redox with oxidases

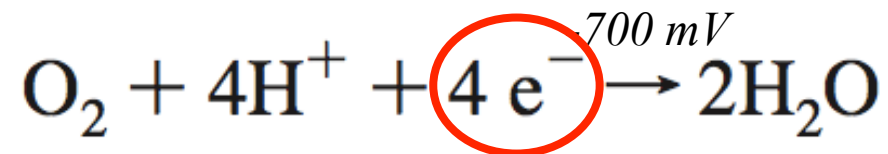
The hydrogen peroxide provide two possible redox reactions. An oxidation:



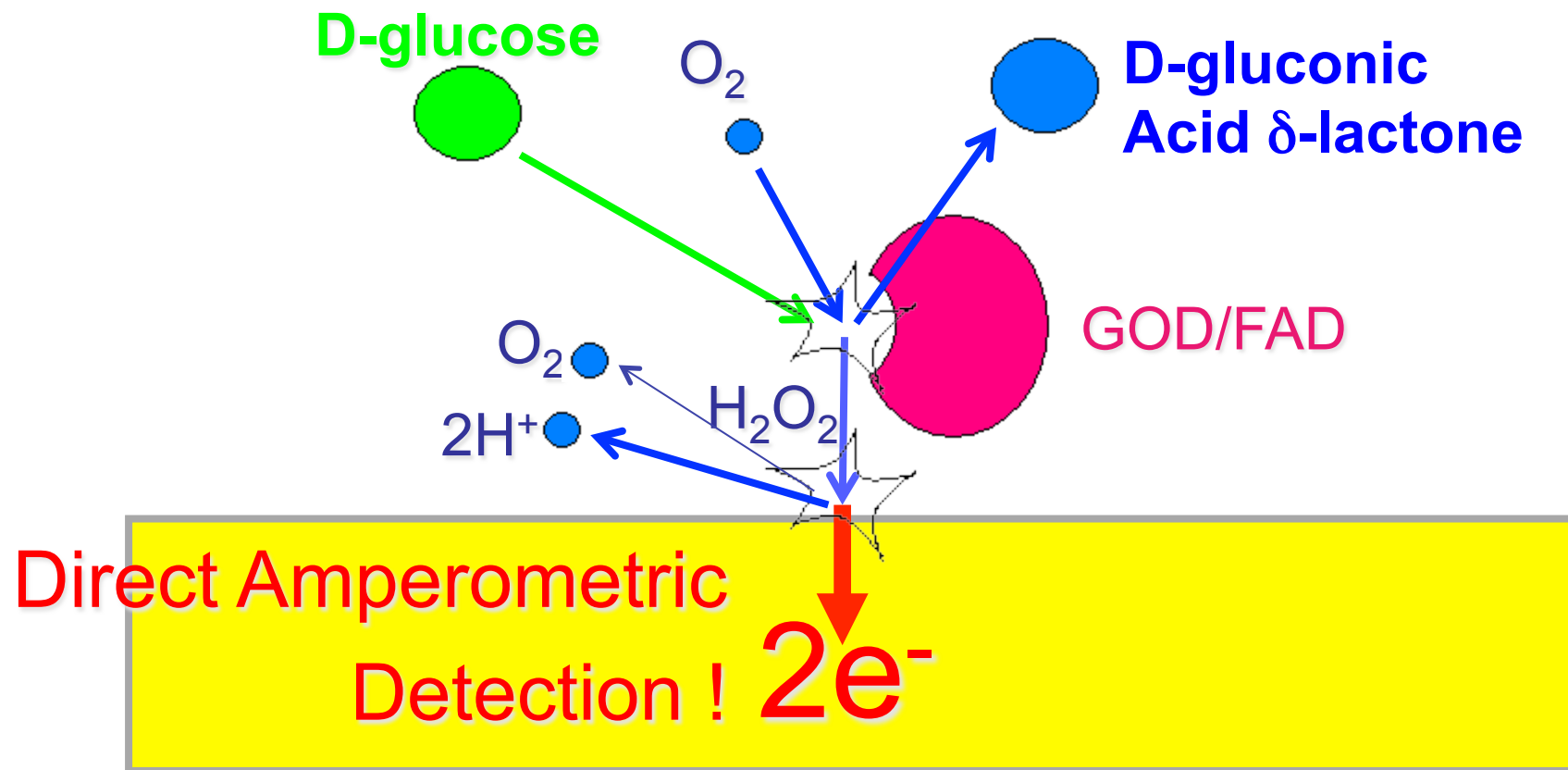
And a reduction:



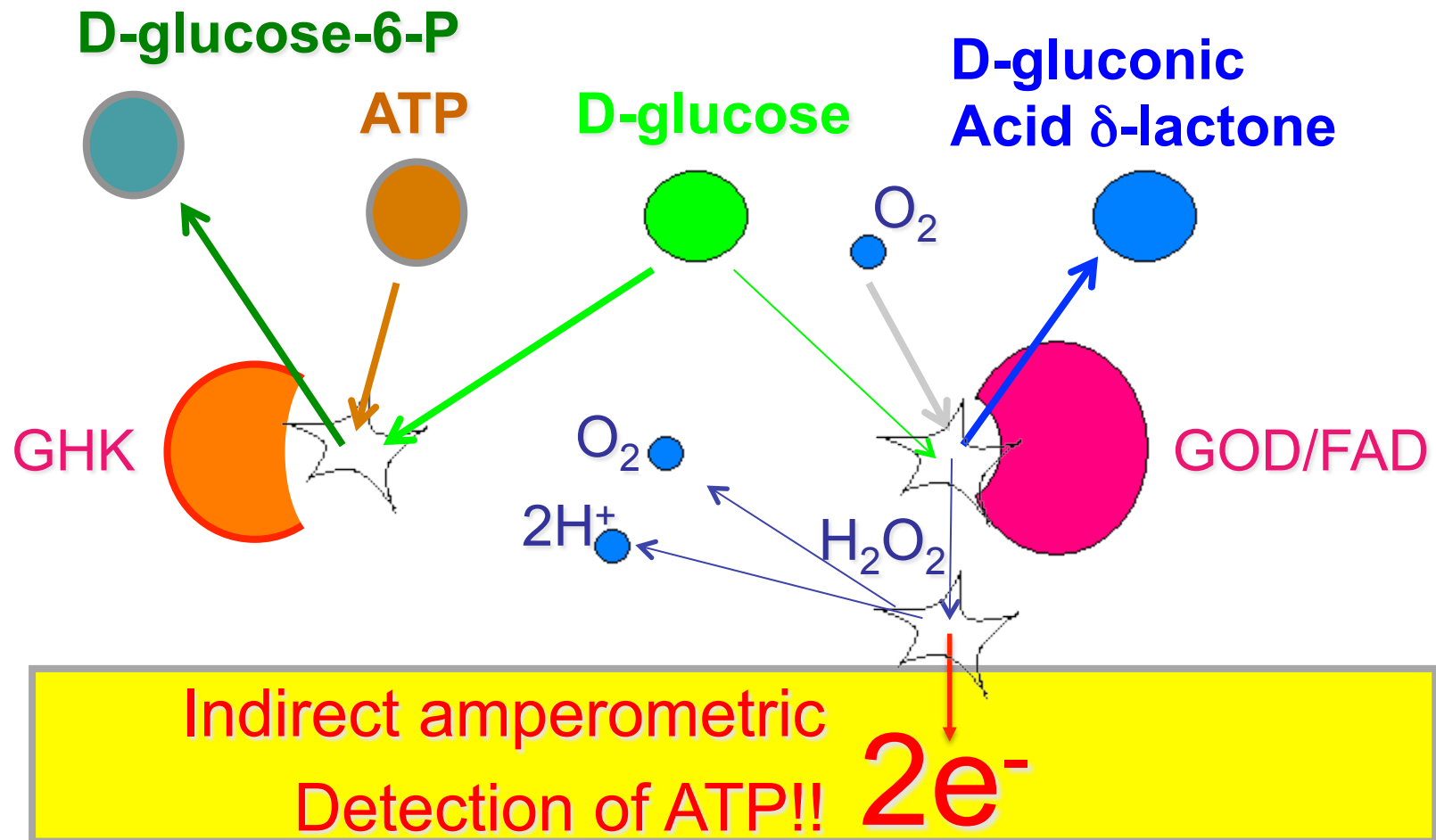
A third redox is provided by the oxygen reduction:



Oxidases based detection

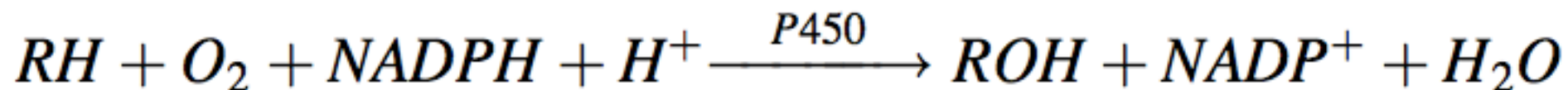


ATP detection

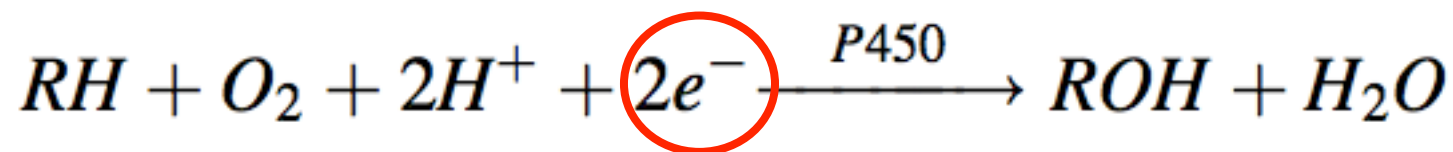


Redox with P450

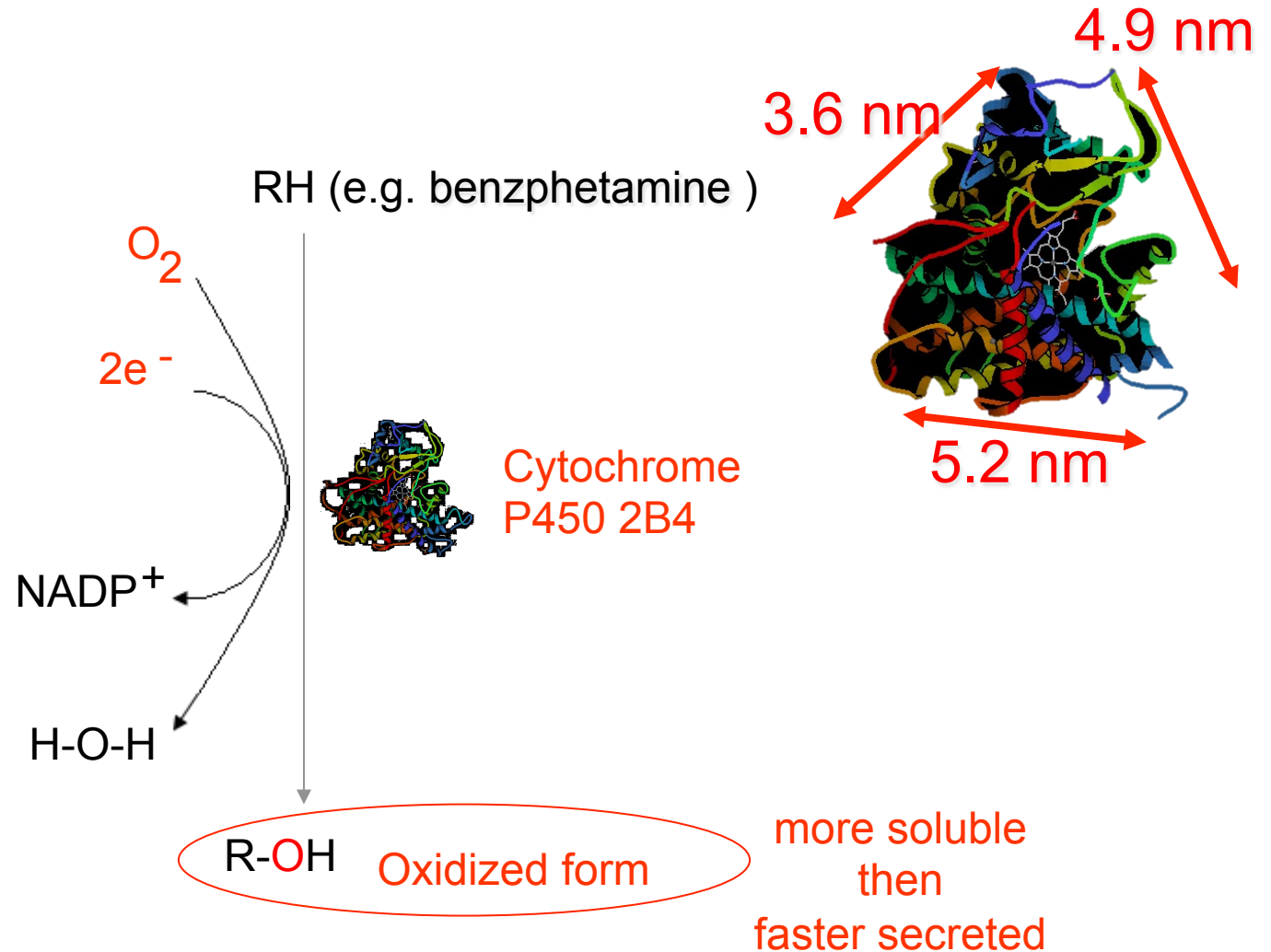
The typical redox involving a cytochrome P450 is as follows:



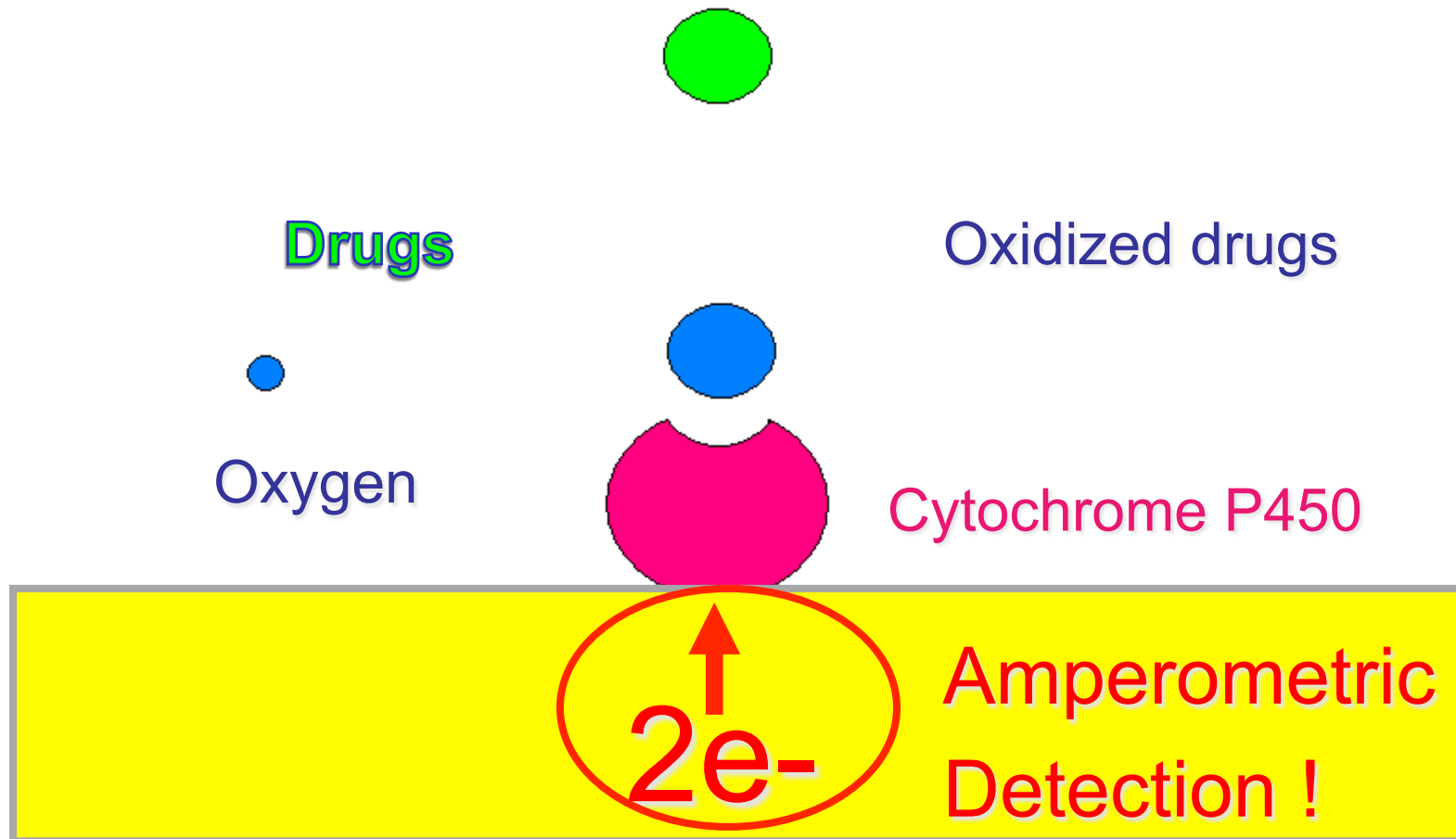
The coenzyme NADPH is mainly providing the need for two electrons required by the drug transformation. Without NADPH, the reaction occurs in water solution using hydrogen ions by water but need two extra electrons:



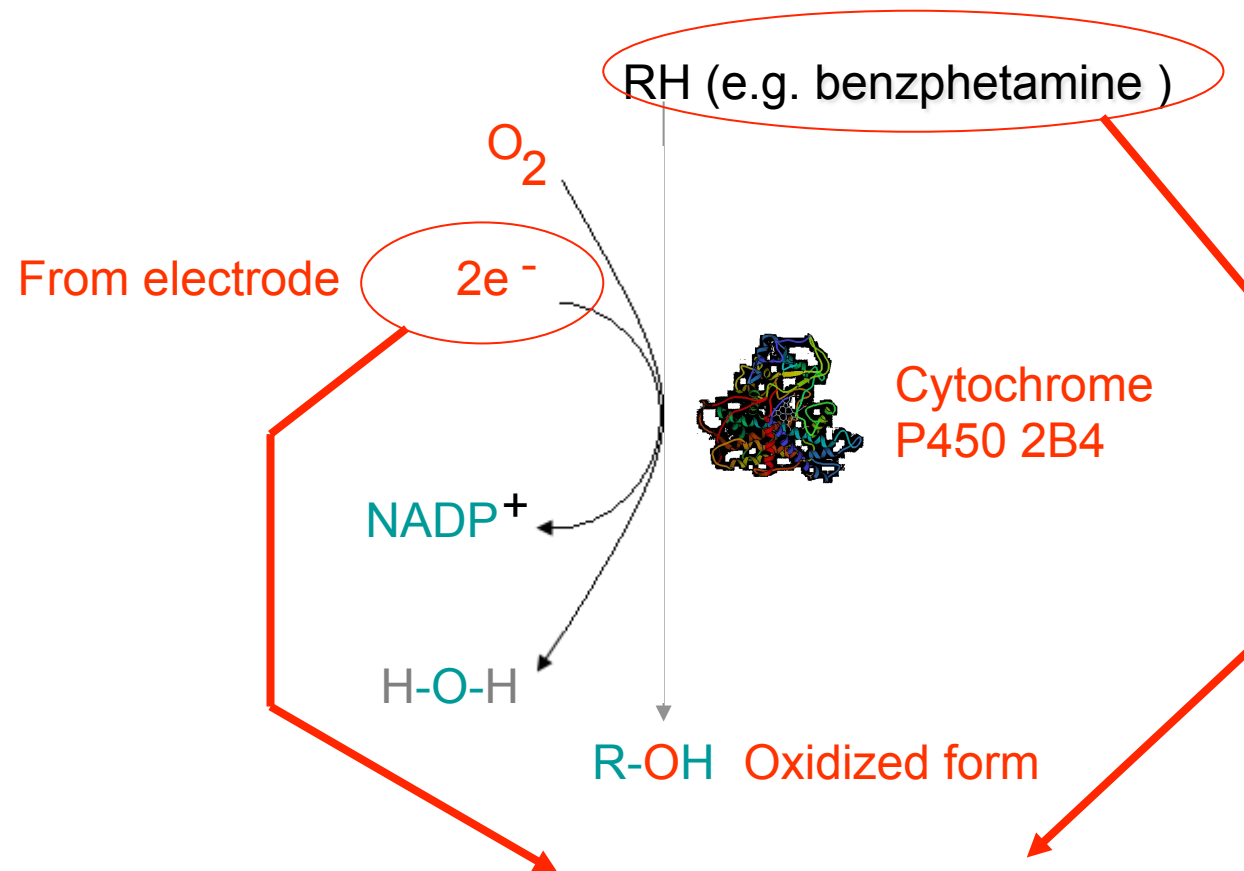
P450 working Principle



P450-based Detection

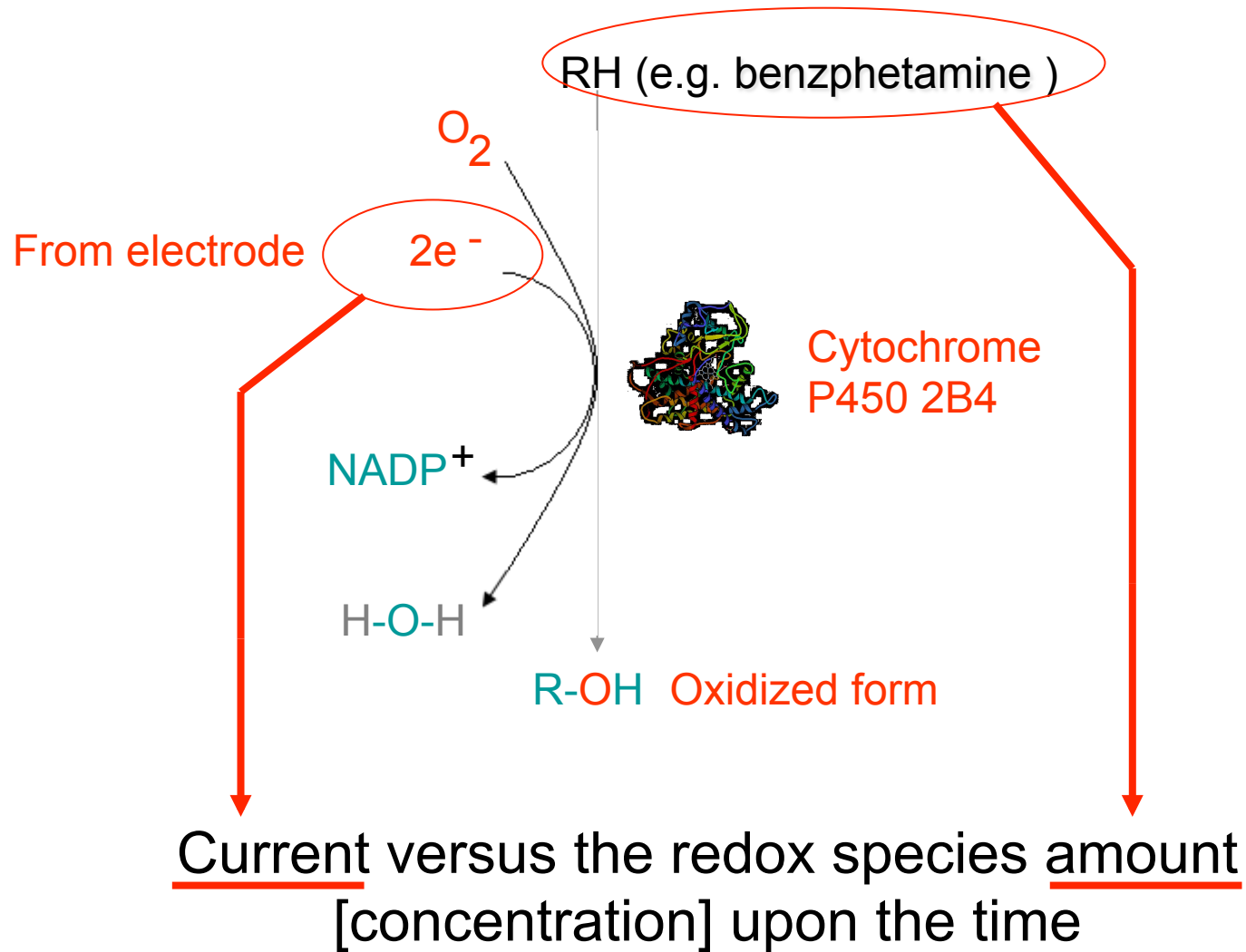


Enzyme based Detection

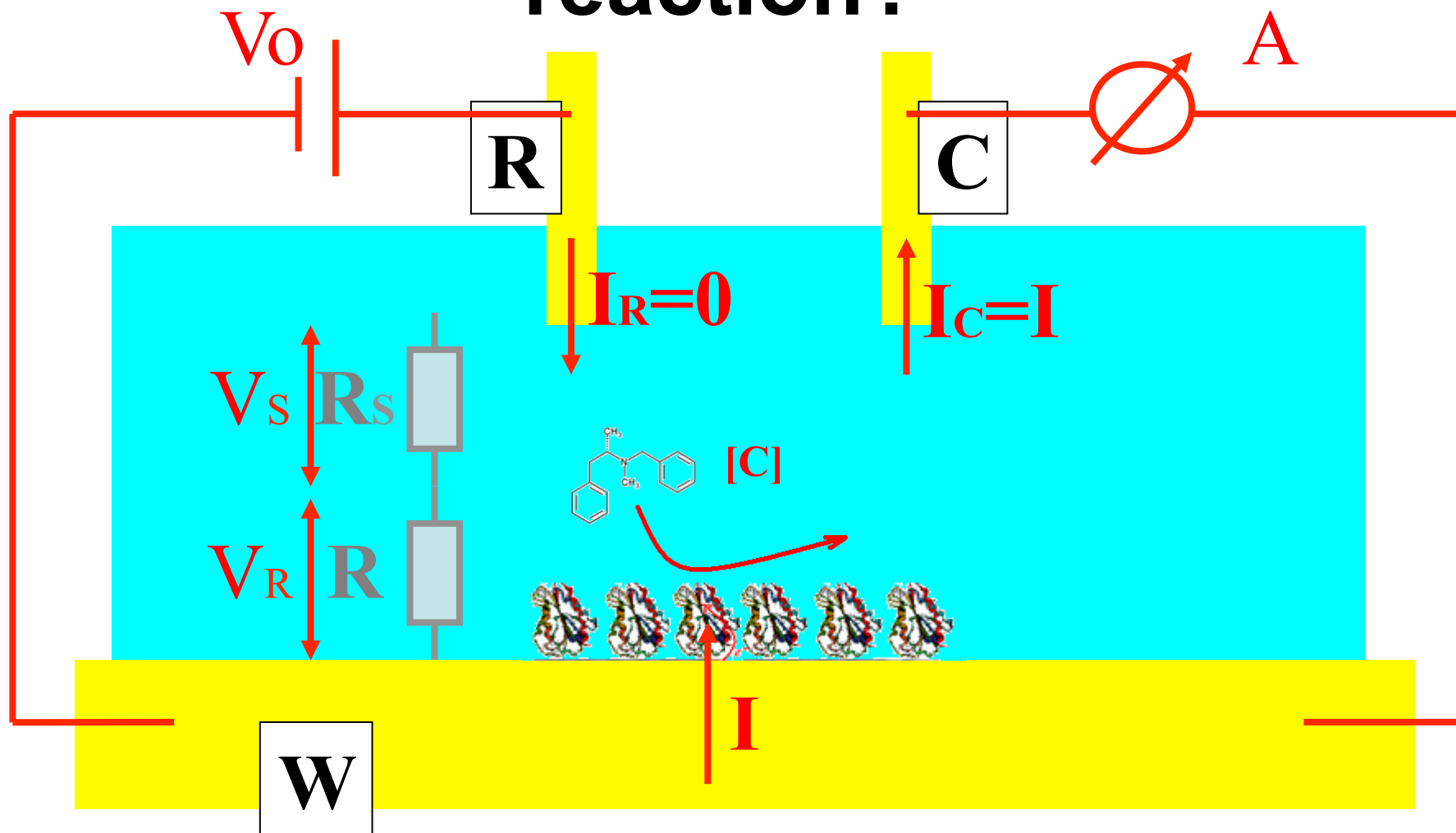


What's about the electro-CHEMICAL properties?

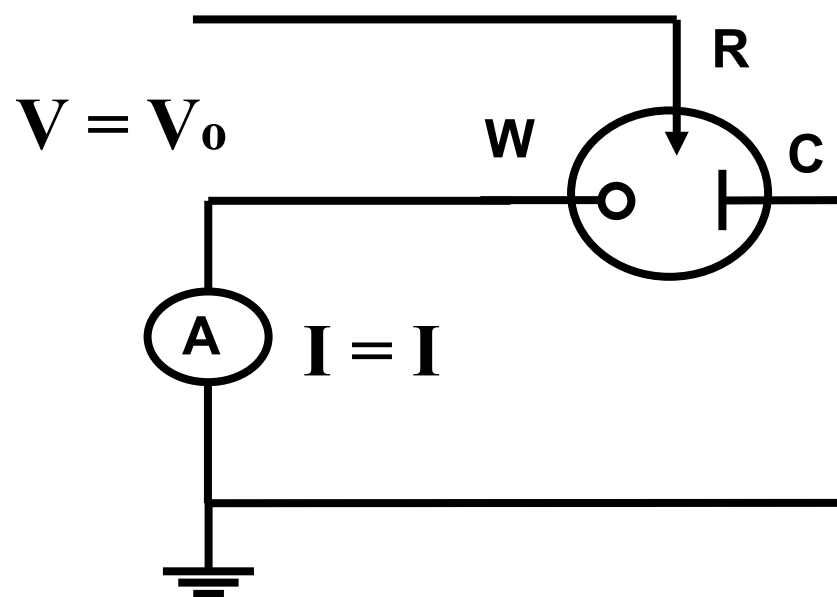
Enzyme based Detection



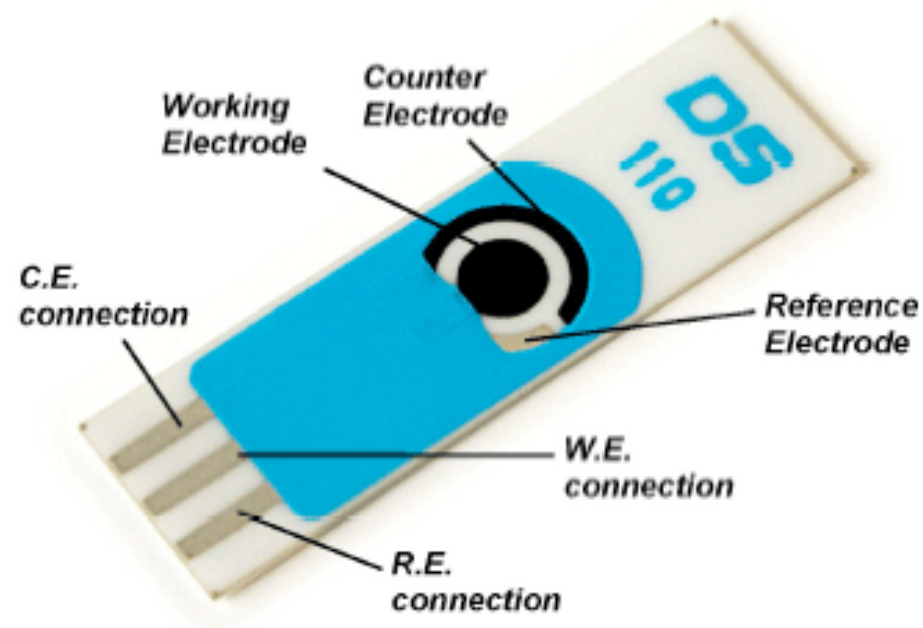
How to measure a redox reaction?



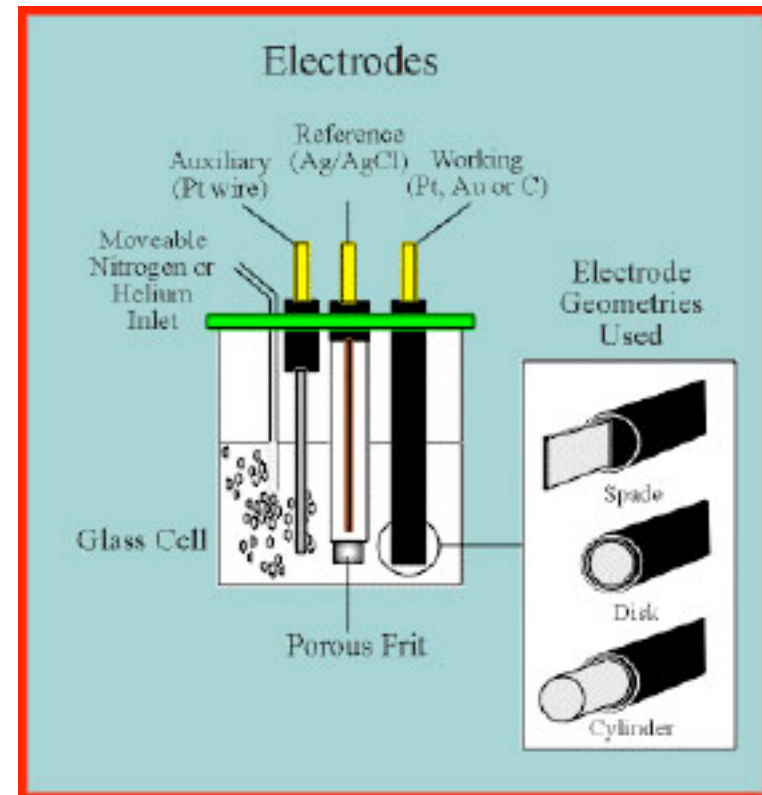
The three-electrode Electrochemical cell



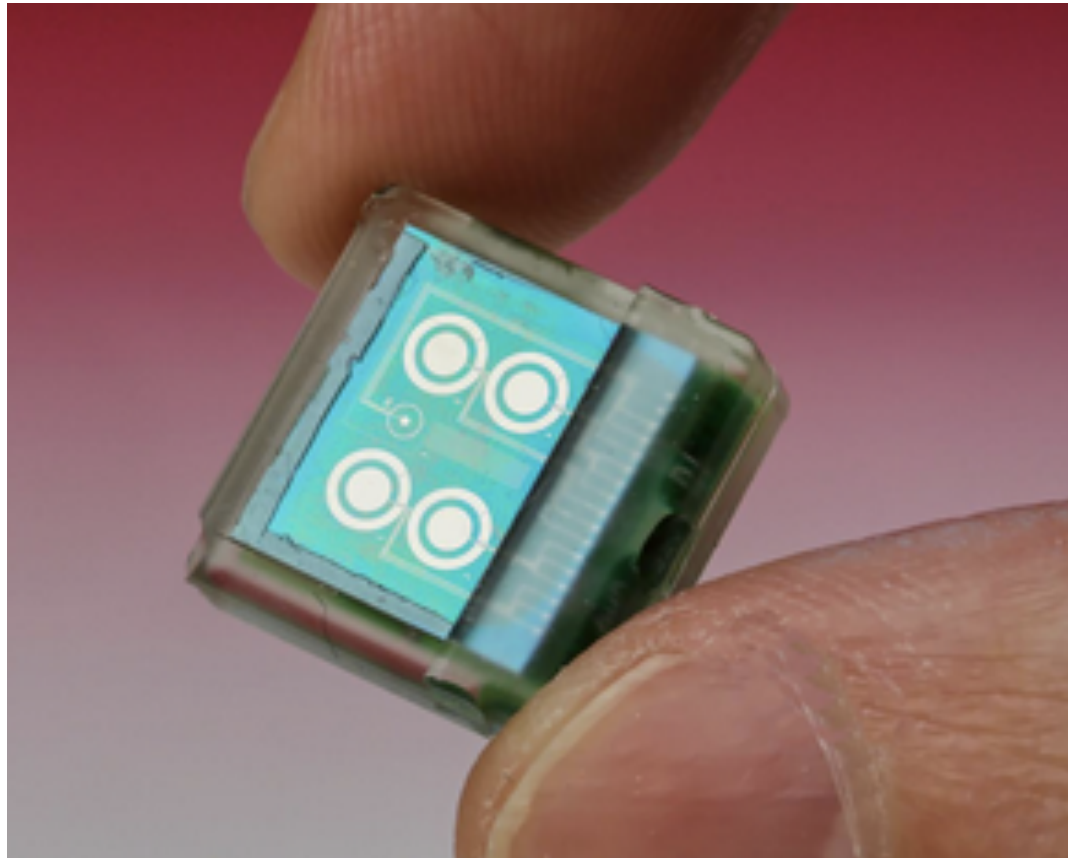
The three-electrode Electrochemical cell



Different kinds of three-electrode Electrochemical cell

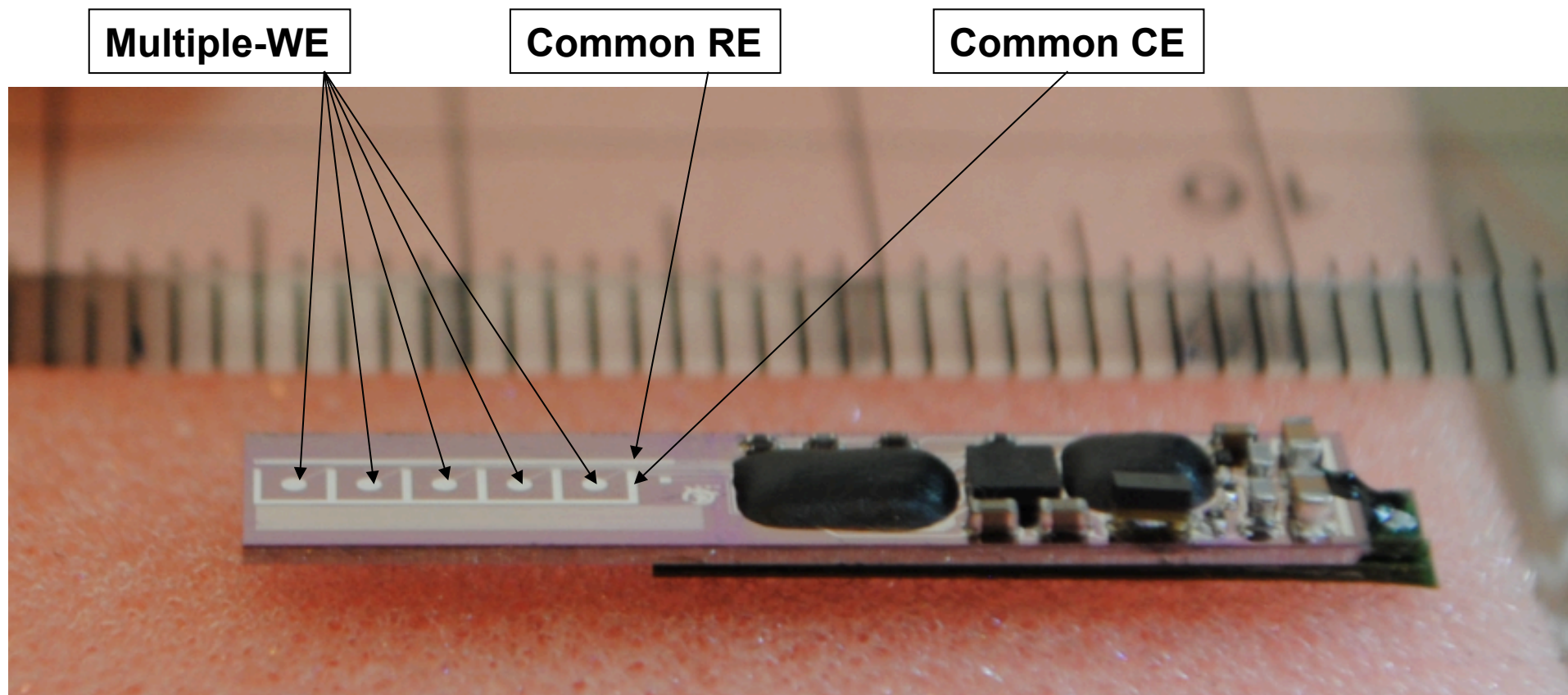


The three-electrode Electrochemical cells

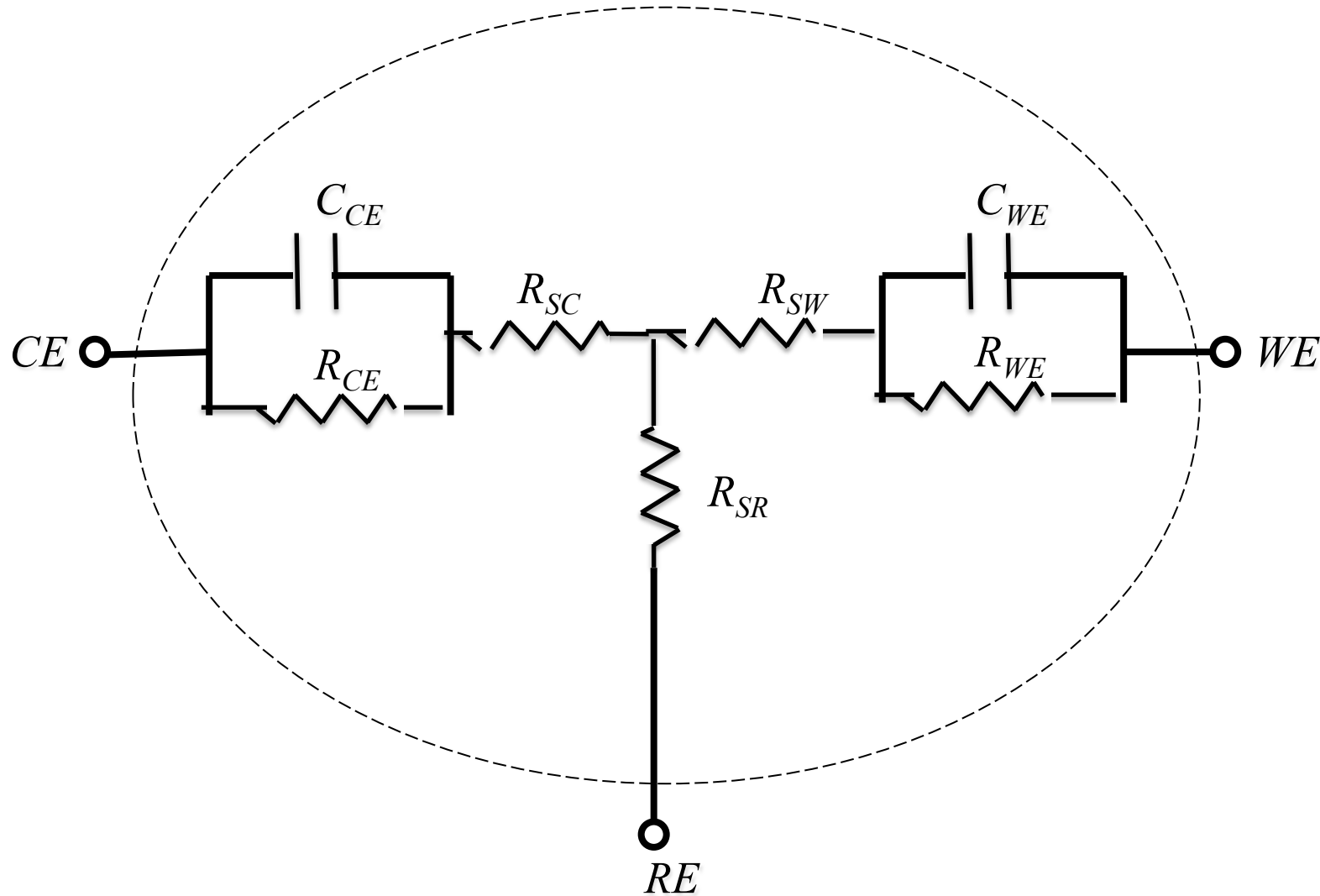


(c) S.Carrara

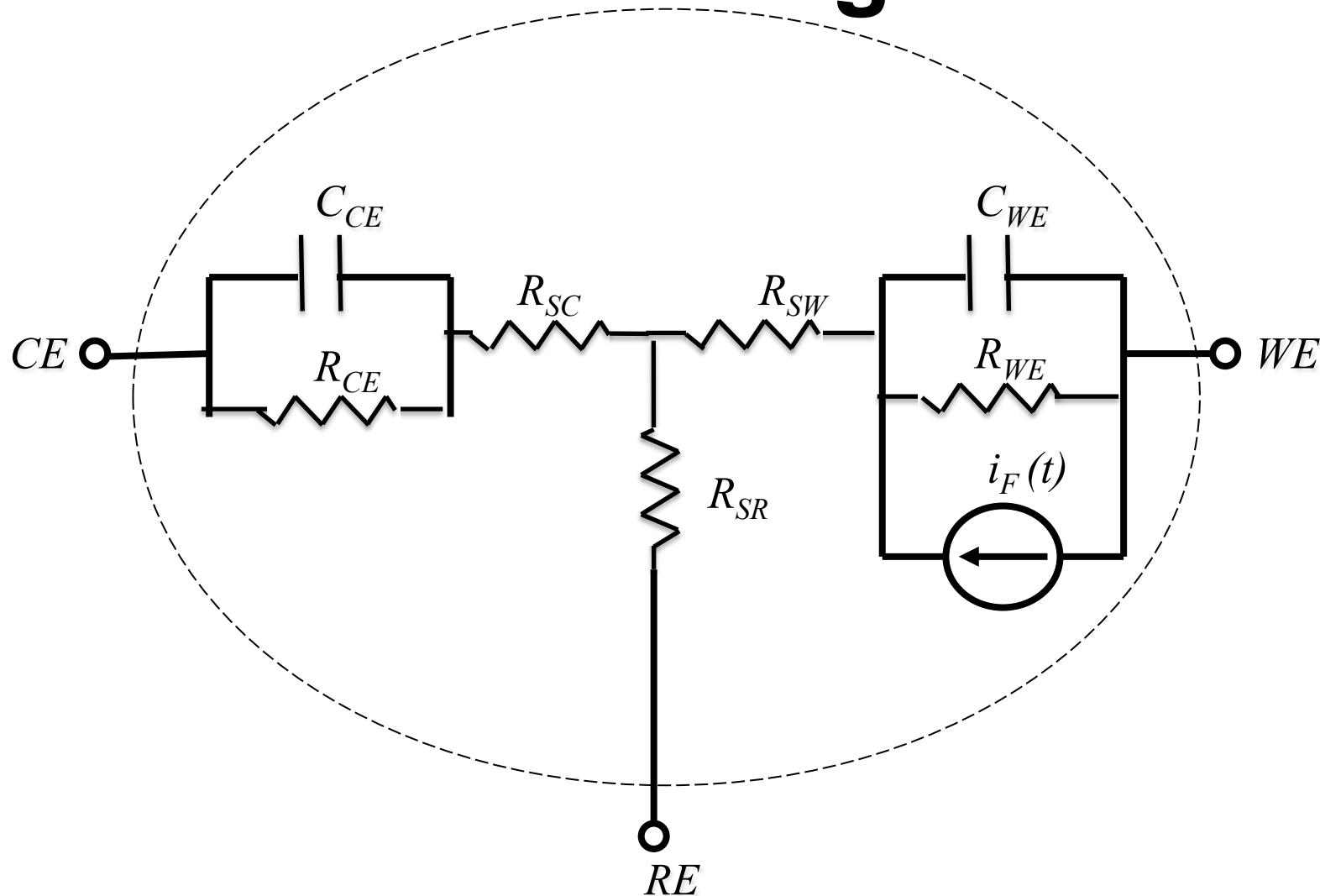
Electrochemical cells with multiple-electrodes



Equivalent circuit

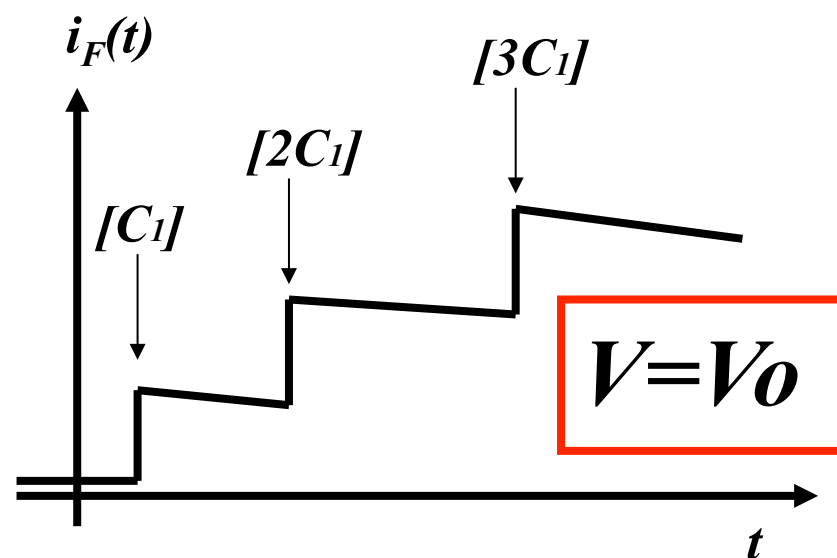


Equivalent circuit with Faradaic current-generator

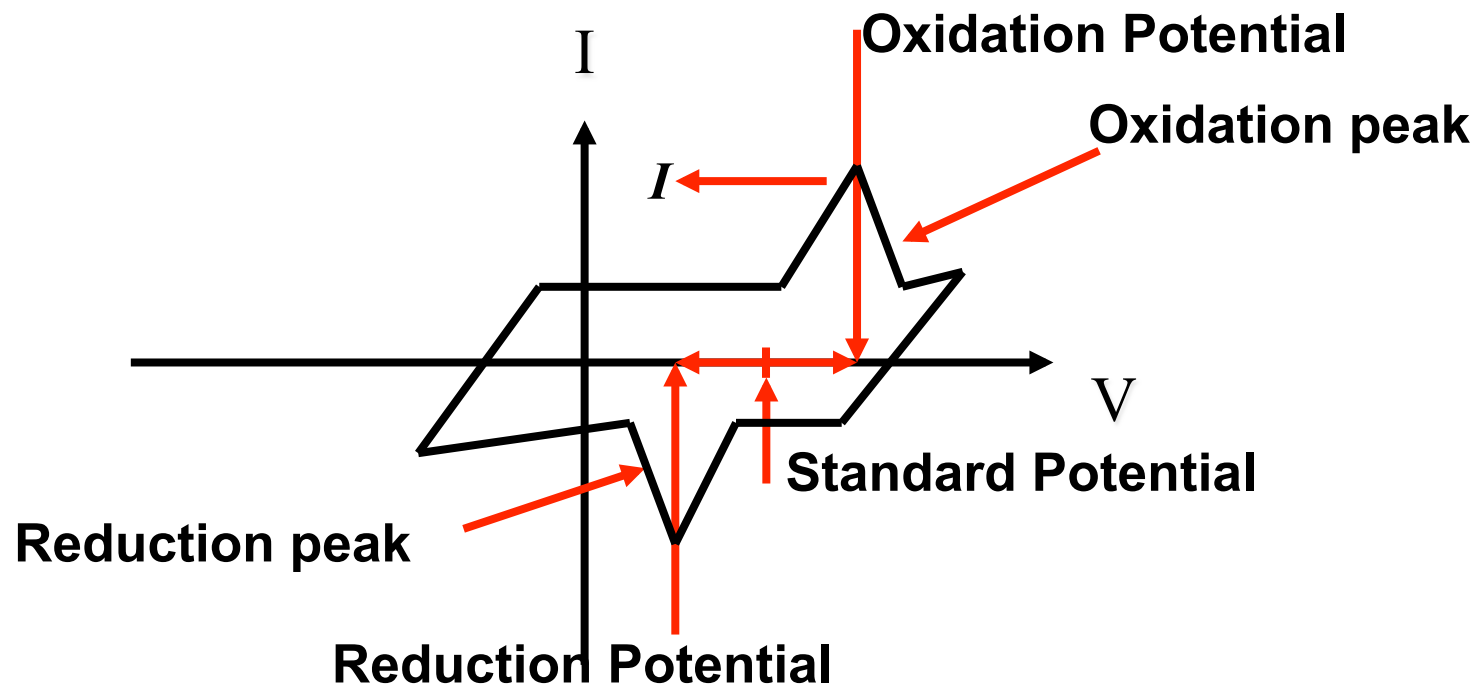


(c) S.Carrara

Faradaic currents from Chrono-Amperometry

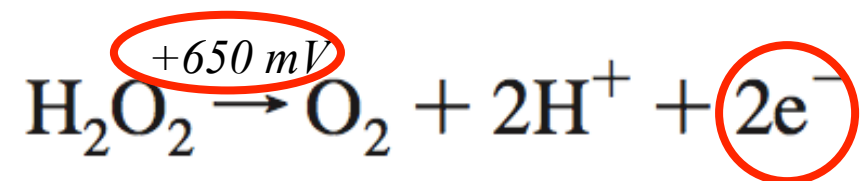


Faradaic currents from Cyclic Voltammetry

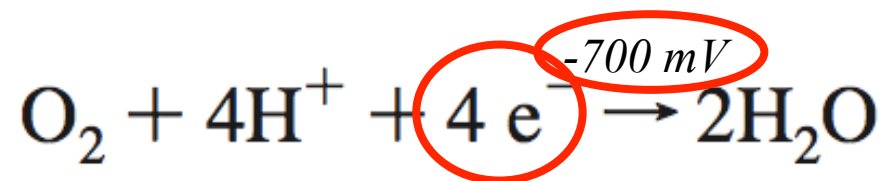


Redox with oxidases

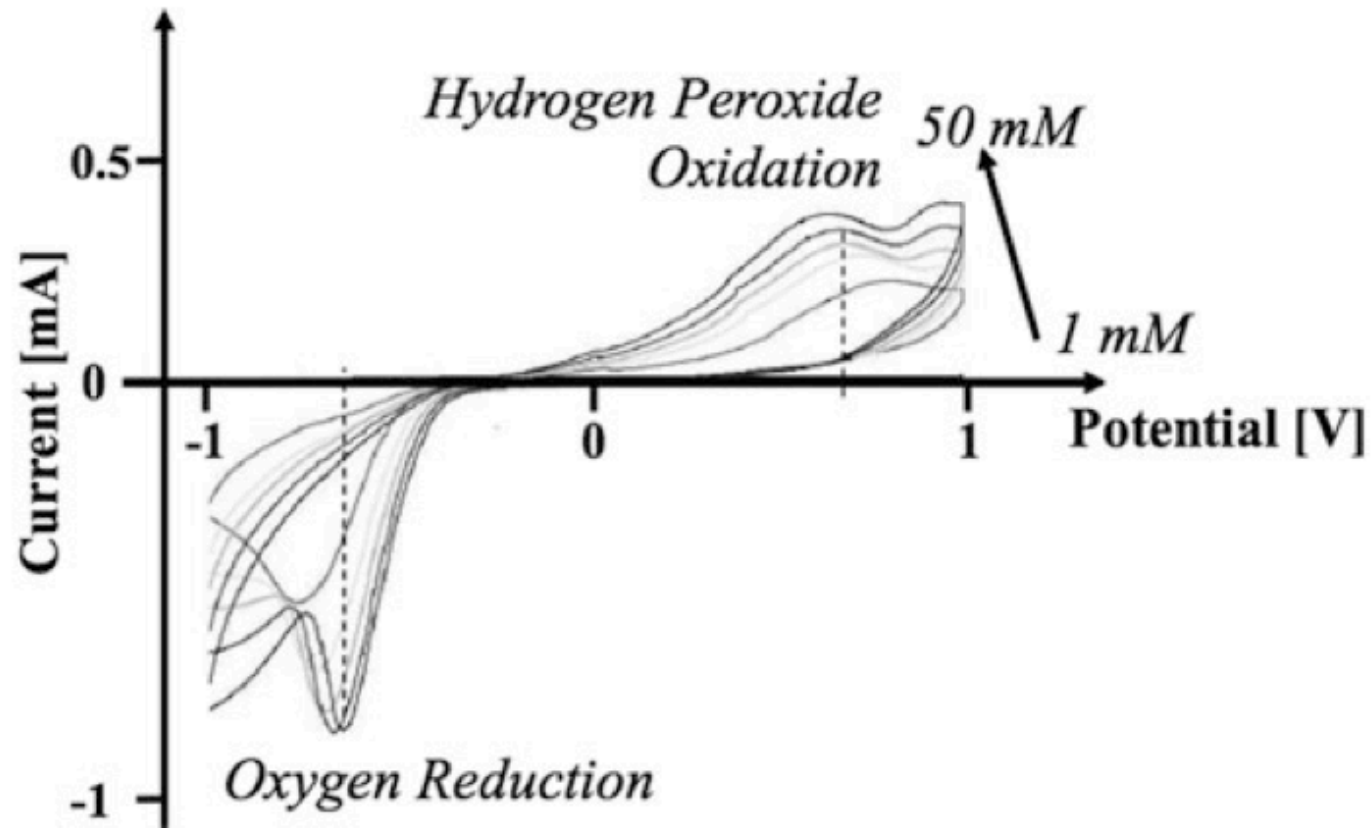
The hydrogen peroxide provides two possible redox reactions.
An oxidation:



And a reduction (of the oxygen):



Redox with hydrogen peroxide



O_2 reduction and H_2O_2 oxidation observed by potential sweeping

Relevant Redox Reactions Equations?

$$V_{I_{MAX}} = f([C]) \quad \text{Nernst equation}$$

$$I = f([C], V) \bigg|_{\frac{dV}{dt} \neq 0} \quad \text{Randles-Sevcik equation}$$

$$I = f([C], t) \big|_{V=Const} \quad \text{Cottrell equation}$$

To derive electrochemical Equations we need of the Laplace' s Transforms

$$F(s) = L_s[f(t)] = \widehat{f}(s) = \int_0^{+\infty} f(t)e^{-st} dt$$

$$L_s[af(t) + bg(t)] = aL_s[f(t)] + bL_s[g(t)] = a\widehat{f}(s) + b\widehat{g}(s)$$

$$L_s[t^n] = \frac{n!}{s^{n+1}}$$

$$L_s\left[\frac{\partial f(t)}{\partial t}\right] = s\widehat{f}(s) - f(0)$$

$$L_s\left[\frac{\partial^2 f(t)}{\partial t^2}\right] = s^2 \widehat{f}(s) - s f(0) - \left[\frac{\partial f(t)}{\partial t}\right]_{t=0}$$

Flick's Laws

The mass flow also has a direction driven by the gradient of concentration (defined by means of the vector differential operator):

$$\vec{j}_m = -D \vec{\nabla} C(\vec{x}, t)$$

In non-vector form (by rotating the x-axis in the direction of the maximum flux and neglecting the variations on y- and z-axes):

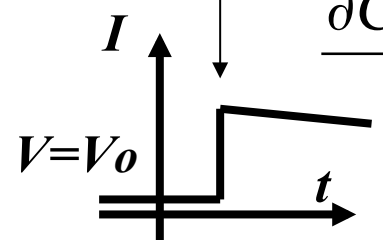
$$j_m \cong -D \frac{\partial C(x, t)}{\partial x}$$

The accumulation rate is provided by the mass flux through a fluidic volume:

$$\frac{\partial C(x, t)}{\partial t} = - \frac{\partial j_m}{\partial x} \longrightarrow \frac{\partial C(x, t)}{\partial t} = D \frac{\partial^2 C(x, t)}{\partial x^2}$$

The Cottrell Equation

$[C_1]$ Linear diffusion equation



$$\frac{\partial C(x,t)}{\partial t} = D \frac{\partial^2 C(x,t)}{\partial x^2} \quad L_s \left[\frac{\partial f(t)}{\partial t} \right] = s\hat{f}(s) - f(0)$$

Boundary conditions

$$s\hat{C}_0(x,s) - C(x,0) = D \frac{\partial \hat{C}_0(x,s)}{\partial x^2}$$

$$\left\{ \begin{array}{l} C(x,0) = C_o \\ \lim_{x \rightarrow \infty} C(x,t) = C_o \\ C(0,t) = 0, t \rightarrow \infty \end{array} \right. \rightarrow C(x,0) = C(x \rightarrow \infty, t) = C_o$$

$$\frac{\partial^2 \hat{C}(x,s)}{\partial x^2} - \frac{s}{D} \hat{C}(x,s) = -\frac{C_o}{D}$$

The Cottrell Equation

$$\frac{\partial^2 \hat{C}(x, s)}{\partial x^2} - \frac{s}{D} \hat{C}(x, s) = -\frac{C_0}{D}$$

$$\hat{C}(x, s) = \frac{C_0}{s} + A(s)e^{-\sqrt{s/D}x} + B(s)e^{+\sqrt{s/D}x}$$

$$\begin{array}{l} \lim_{x \rightarrow \infty} C(x, t) = C_0 \\ L_s[t^n] = \frac{n!}{s^{n+1}} \end{array} \longrightarrow \lim_{x \rightarrow \infty} \hat{C}(x, s) = \frac{C_0}{s}$$

$$B(s) = 0, \text{ while } \hat{C}(x, s) = \frac{C_0}{s} + A(s)e^{-\sqrt{s/D}x}$$

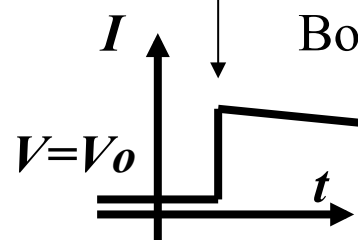
The Cottrell Equation

$[C_1]$ Linear diffusion equation

Boundary conditions $\hat{C}_0(x, s) = \frac{C_0}{s} + A(s)e^{-\sqrt{s/D}x}$

By definition

$V=V_o$



By definition

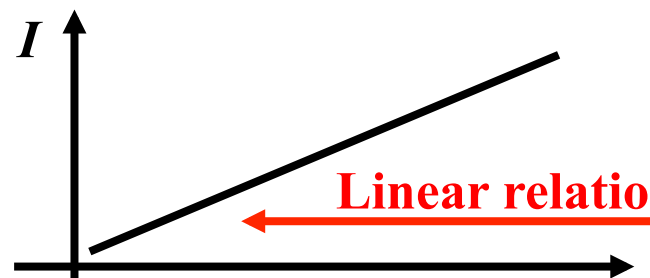
$$j(x, t) = \frac{i(t)}{A} = nFD \left[\frac{\partial C(x, t)}{\partial x} \right]_{x=0}$$

$$\frac{\hat{i}(s)}{nFA} = D \frac{\partial \hat{C}(x, s)}{\partial x} \bigg|_{x=0}$$

$$\hat{i}(s) = nFA \frac{\sqrt{DC_0}(x, s)}{\sqrt{s}}$$

Cottrell equation

Linear relationship



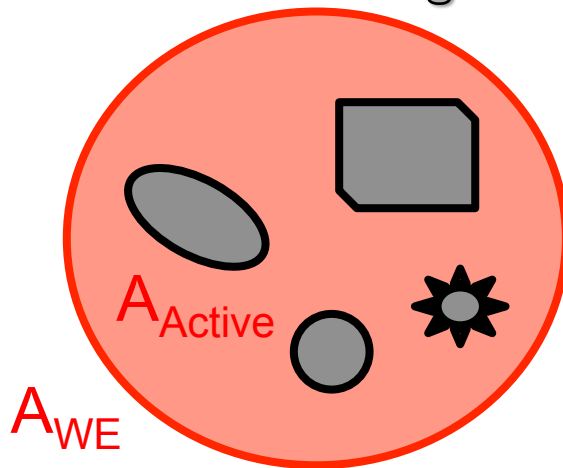
$$i(x, t) = \frac{nFA\sqrt{DC(x, t)}}{\sqrt{\pi t}}$$

Geometrical Area vs Active Area

$$i(x,t) = \frac{nFA\sqrt{DC(x,t)}}{\sqrt{\pi t}}$$

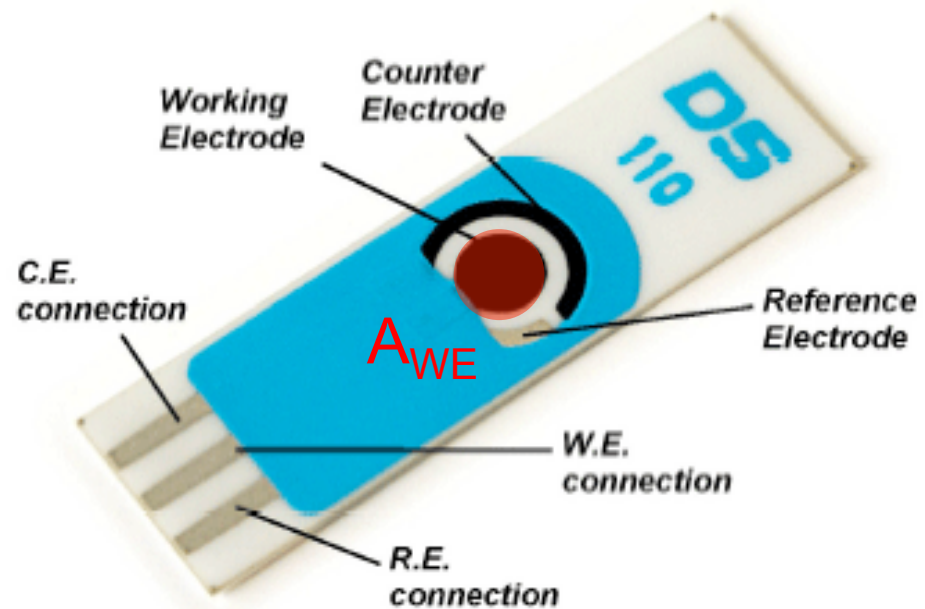
?

Non Active Regions



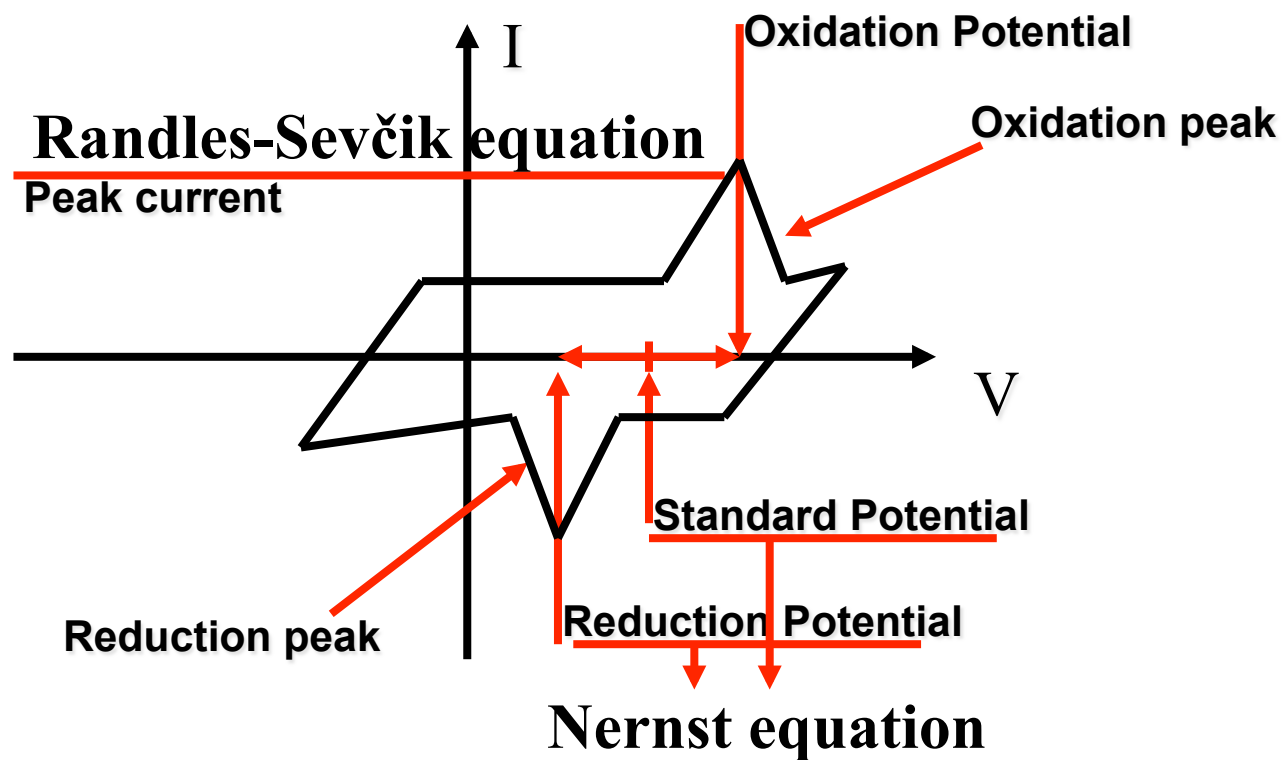
$$A_{Active} < A_{WE}$$

Electrochemically Active Area

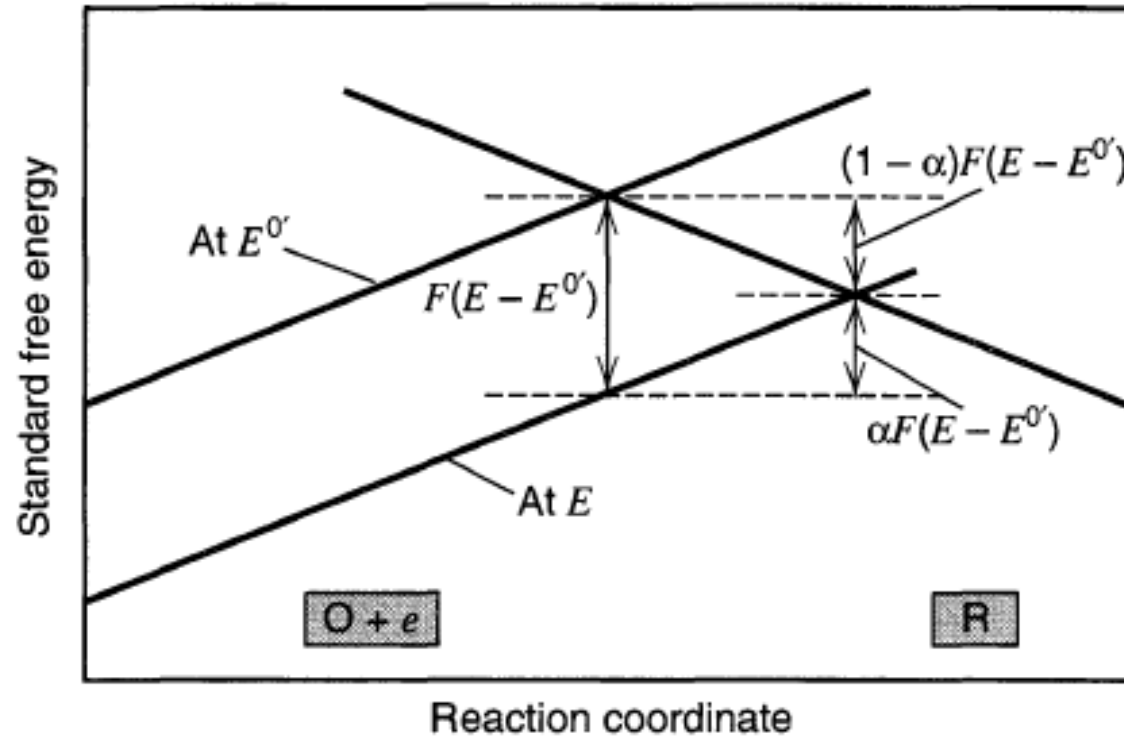


$$i(x,t) = \frac{nFA_{Active}\sqrt{DC(x,t)}}{\sqrt{\pi t}}$$

Redox reactions from Voltammetry

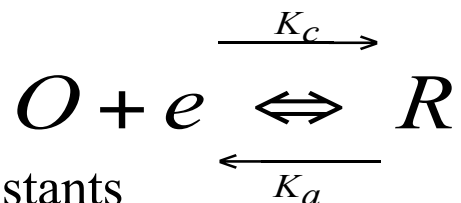


Redox Reactions



Nernst Equation

Redox Reaction



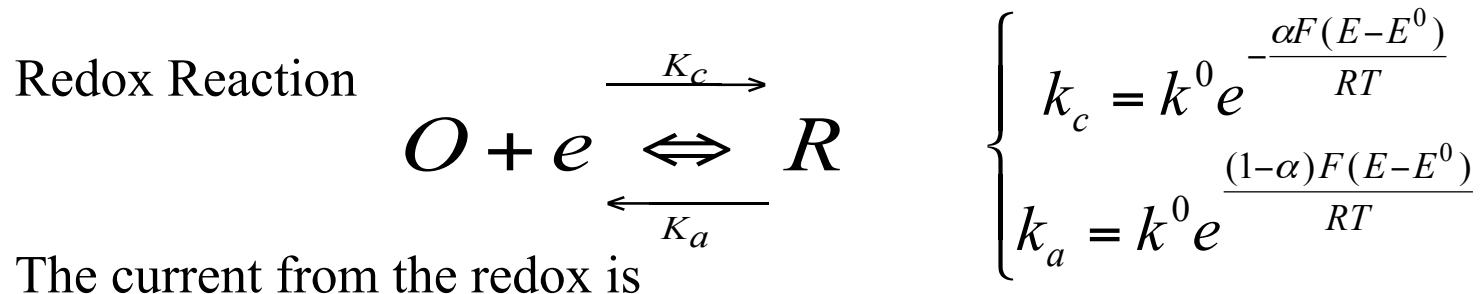
Equilibrium Constants

$$\begin{cases} k_c = k_c^0 e^{-\frac{\Delta G_c}{RT}} = k_c^0 e^{-\frac{\Delta G_c^0 + \alpha F(E-E^0)}{RT}} \\ k_a = k_a^0 e^{-\frac{\Delta G_a}{RT}} = k_a^0 e^{-\frac{\Delta G_a^0 - (1-\alpha)F(E-E^0)}{RT}} \end{cases} = \boxed{k_c^0 e^{-\frac{\Delta G_c^0}{RT}} e^{-\frac{\alpha F(E-E^0)}{RT}}}$$

@ Equilibrium:

$$E = 0; \alpha = 0.5; k_c = k_a \Rightarrow k_c^0 e^{-\frac{\Delta G_c^0}{RT}} = k_c^0 e^{-\frac{\Delta G_c^0}{RT}} = k^0$$

Nernst Equation



$$i = i_c - i_a = nFA[k_c C_O(0,t) - k_a C_R(0,t)]$$

$$i = FAk^0 \left[C_O(0,t) e^{-\frac{\alpha F(E-E^0)}{RT}} - C_R(0,t) e^{\frac{(1-\alpha)F(E-E^0)}{RT}} \right]$$

@ Equilibrium:

$$i = 0 \Rightarrow C_O(0,t) e^{-\frac{\alpha F(E-E^0)}{RT}} = C_R(0,t) e^{\frac{(1-\alpha)F(E-E^0)}{RT}}$$

Nernst Equation

@ Equilibrium:

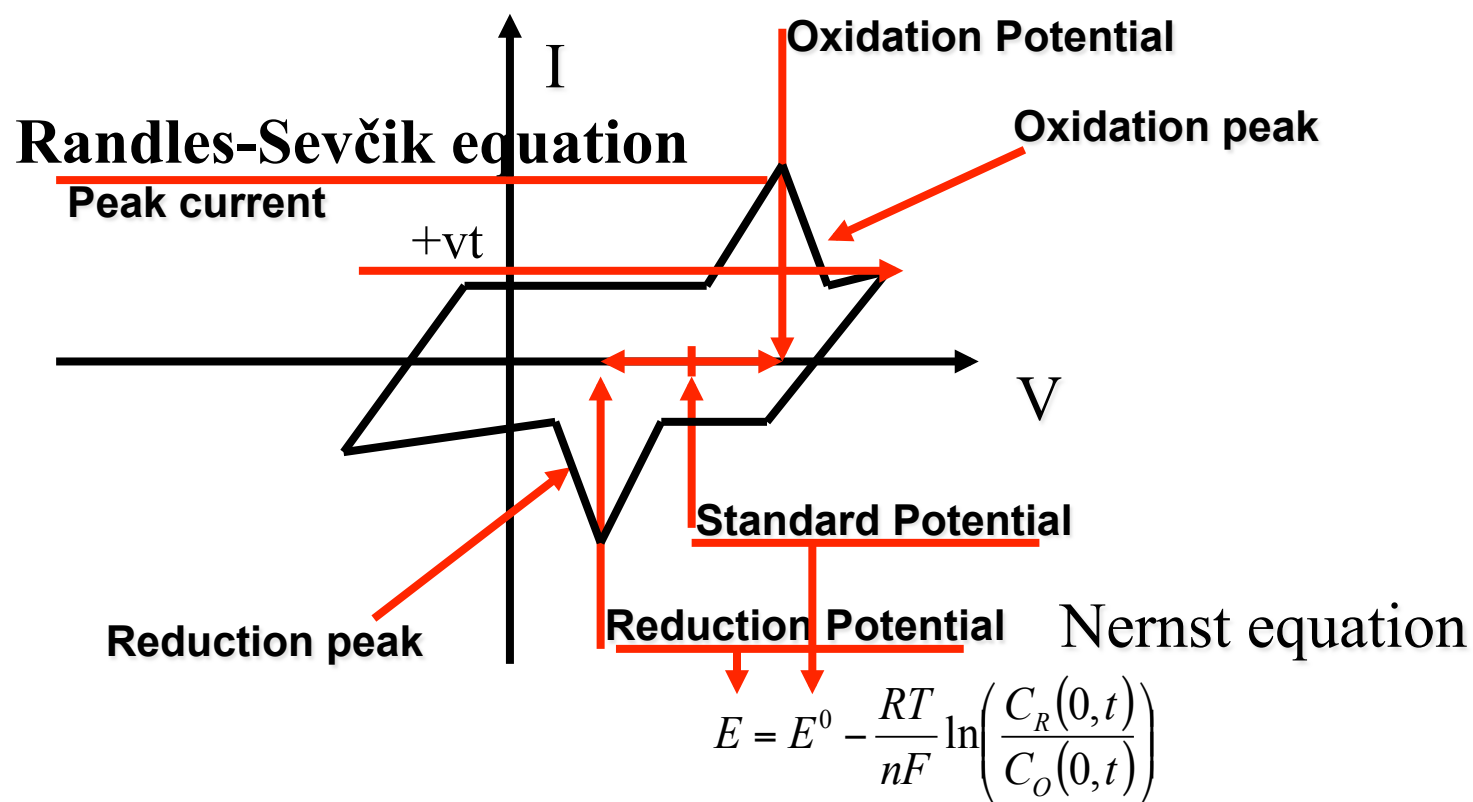
$$i = 0 \Rightarrow C_O(0, t) e^{-\frac{\alpha F(E - E^0)}{RT}} = C_R(0, t) e^{\frac{(1-\alpha)F(E - E^0)}{RT}}$$

$$i = 0 \Rightarrow \frac{C_O(0, t)}{C_R(0, t)} = e^{\frac{F(E - E^0)}{RT}} \Rightarrow \frac{F(E - E^0)}{RT} = \ln \left[\frac{C_O(0, t)}{C_R(0, t)} \right]$$

$$E = E^0 + \frac{RT}{nF} \ln \left[\frac{C_O(0, t)}{C_R(0, t)} \right] \text{ Nernst equation}$$

If n electrons are involved!

Redox reactions from Voltammetry



Randles-Sevcik Equation

Voltage Sweep

$$E = E_i + vt$$

$$\frac{C_O(0,t)}{C_R(0,t)} = e^{\frac{F(E+vt-E^0)}{RT}}$$

$$\hat{C}_0(x,s) = \frac{C_0}{s} + A(s)e^{-\sqrt{s/D}x}$$

$$j(x,t) = \frac{i(t)}{A} = nFD \left[\frac{\partial C(x,t)}{\partial x} \right]_{x=0} \Rightarrow i(t) = nFAD \left[\frac{\partial C(x,t)}{\partial x} \right]_{x=0}$$

$$\left[\frac{\partial C(x,t)}{\partial x} \right]_{i=i_{peak}} \propto \sqrt{\frac{nFDv}{RT}} C(0,t) \Rightarrow i(t) = nFAD \sqrt{\frac{nFDv}{RT}} C(0,t)$$

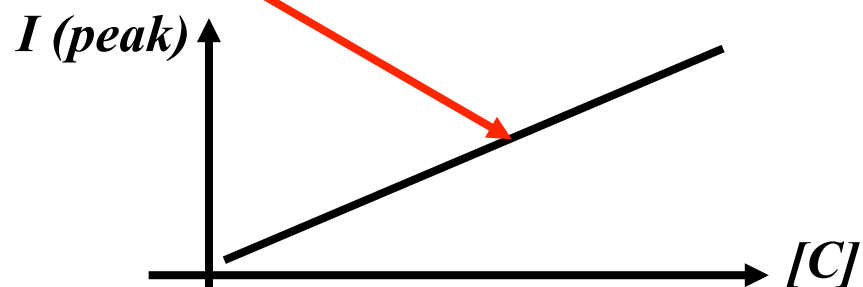
Randles-Sevčik Equation

Voltage Sweep

$$E = E_i + vt$$

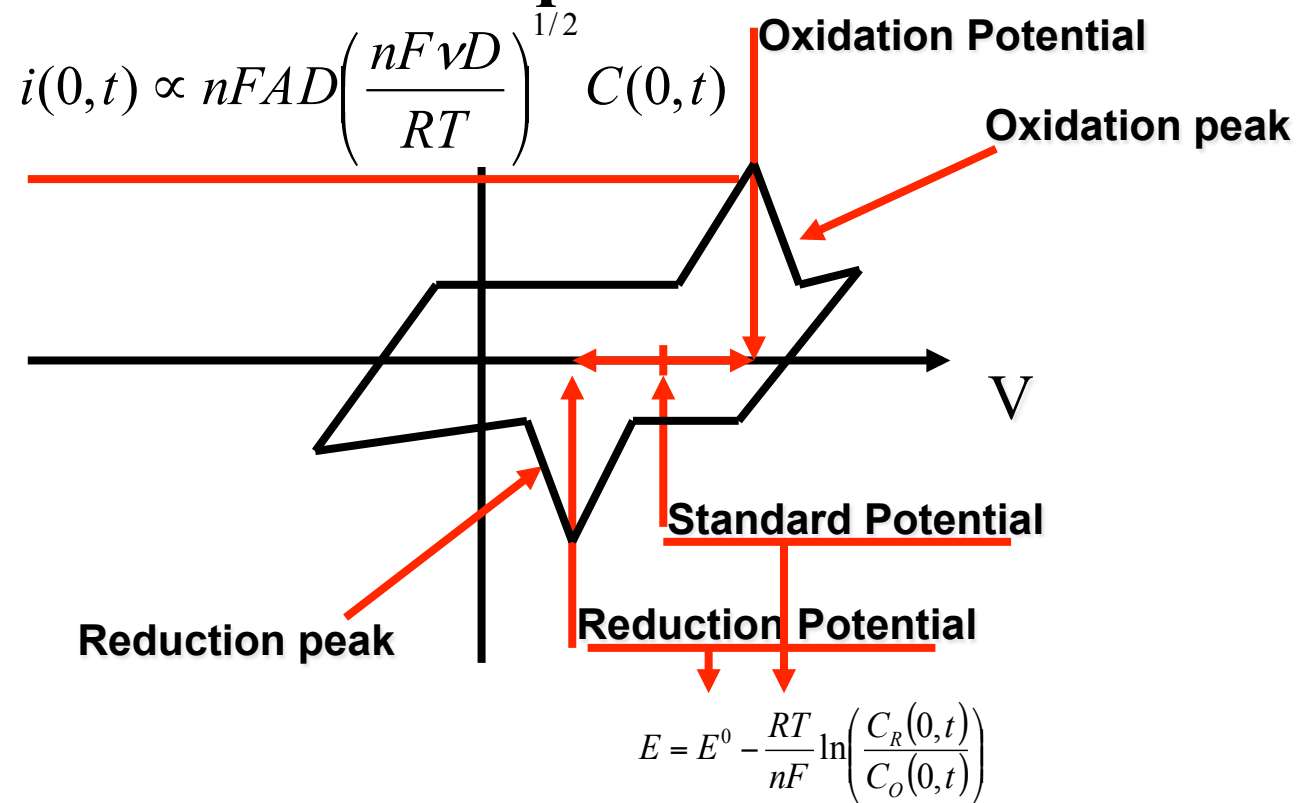
$$\frac{C_o(0,t)}{C_R(0,t)} = e^{\frac{F(E+vt-E^0)}{RT}}$$

$$i(t) = nFAD\sqrt{\frac{nFDv}{RT}} C(0,t)$$



Redox reactions from Voltammetry

Randles-Sevcik equation for the Peak current



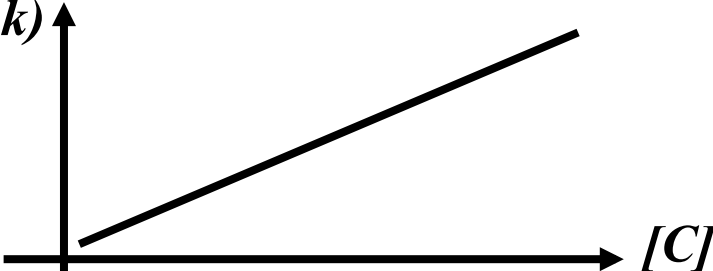
Nernst equation

Detection Principle

- Sensitivity: definition

$$i(t) = nFAD\sqrt{\frac{nFDv}{RT}}C(0,t)$$

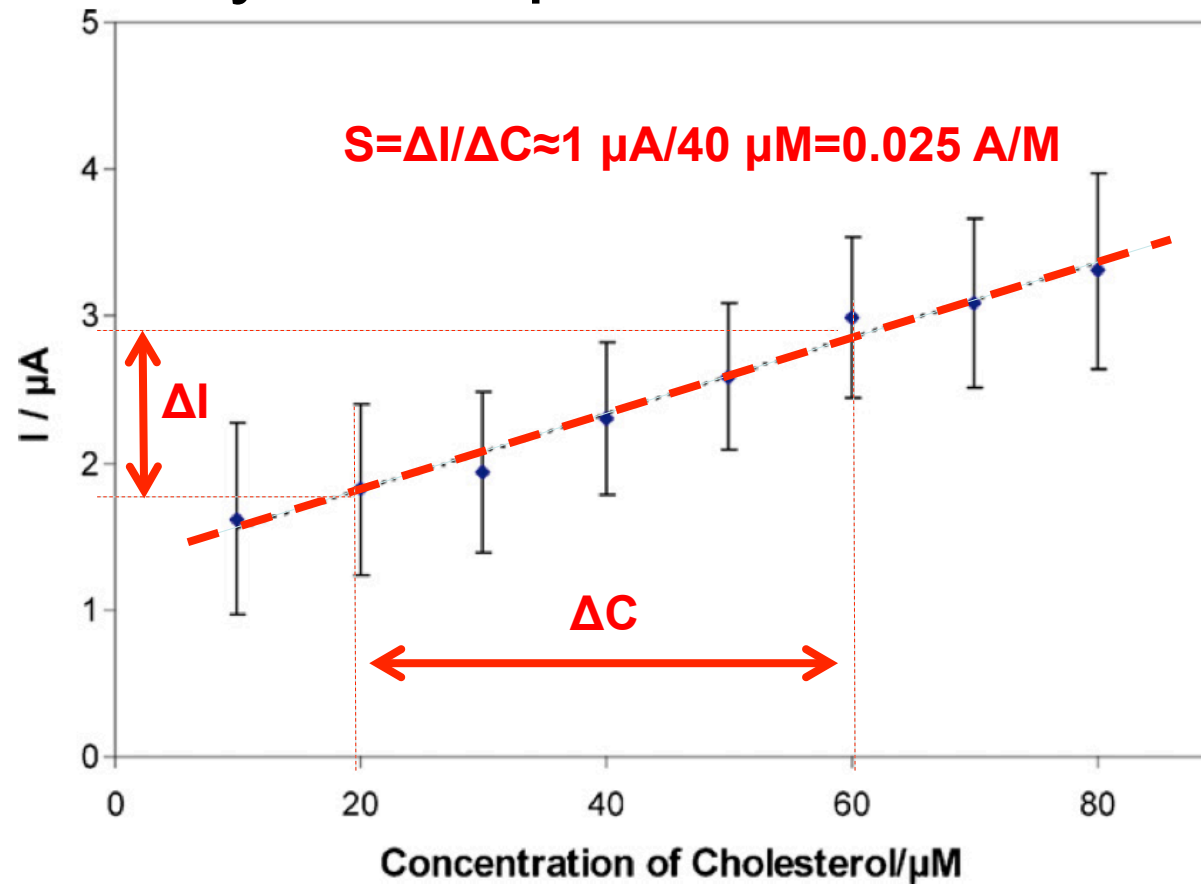
I (peak)


$$\Delta i = nFAD\sqrt{\frac{nFDv}{RT}}\Delta C \rightarrow \frac{\Delta i}{\Delta C} \equiv S$$

Detection Sensitivity!

Detection Principle

- Sensitivity: example – A linear sensor



Detection Principle

- Sensitivity: metric considerations

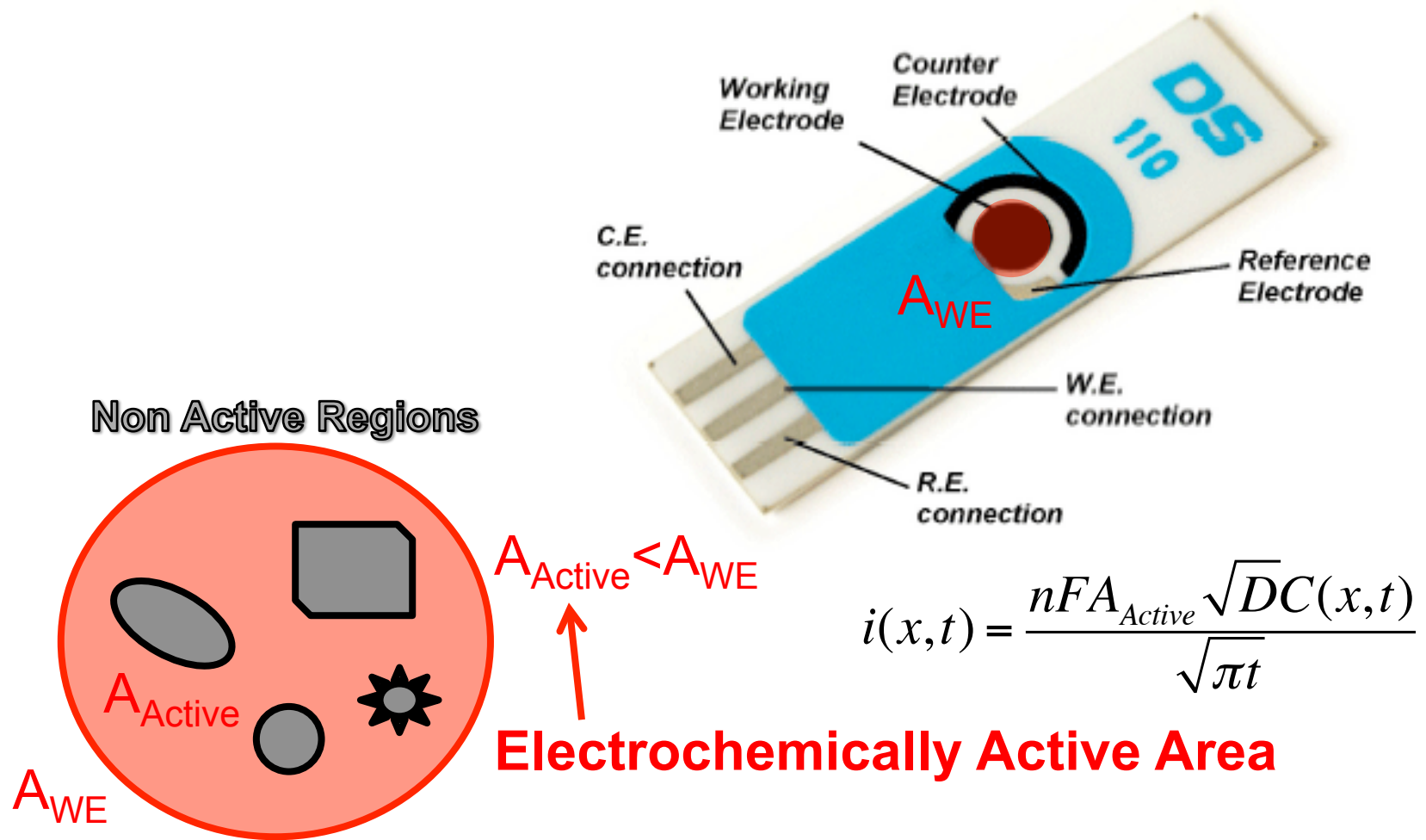
$$S = \frac{\Delta i}{\Delta C} = \frac{1 \mu A}{40 \mu M} = 25 \frac{mA}{M}$$

Mathematically correct, but are we going to measure mAmpere each Molar of concentration?

$$S = \frac{\Delta i}{\Delta C} = \frac{1 \mu A}{40 \mu M} = 25 \frac{nA}{\mu M}$$

More correct, because we are going to require a precision of sub- μ Ampere meanwhile facing variations on μ M range

Geometrical Area vs Active Area



Detection Principle

- Sensitivity: metric considerations

$$S = \frac{\Delta i}{\Delta C} = \frac{1 \mu A}{40 \mu M} = 25 \frac{mA}{M}$$

Correct, but we cannot compare biosensors with different geometry on working electrodes

$$S_A = \frac{\Delta i}{\Delta C \cdot A_{WE}} = \frac{1 \mu A}{40 \mu M \cdot 0.2 cm^2} = 125 \frac{nA}{\mu M \cdot cm^2}$$

More useful to compare biosensors with different geometry on working electrodes

Sensitivity per Unit Area

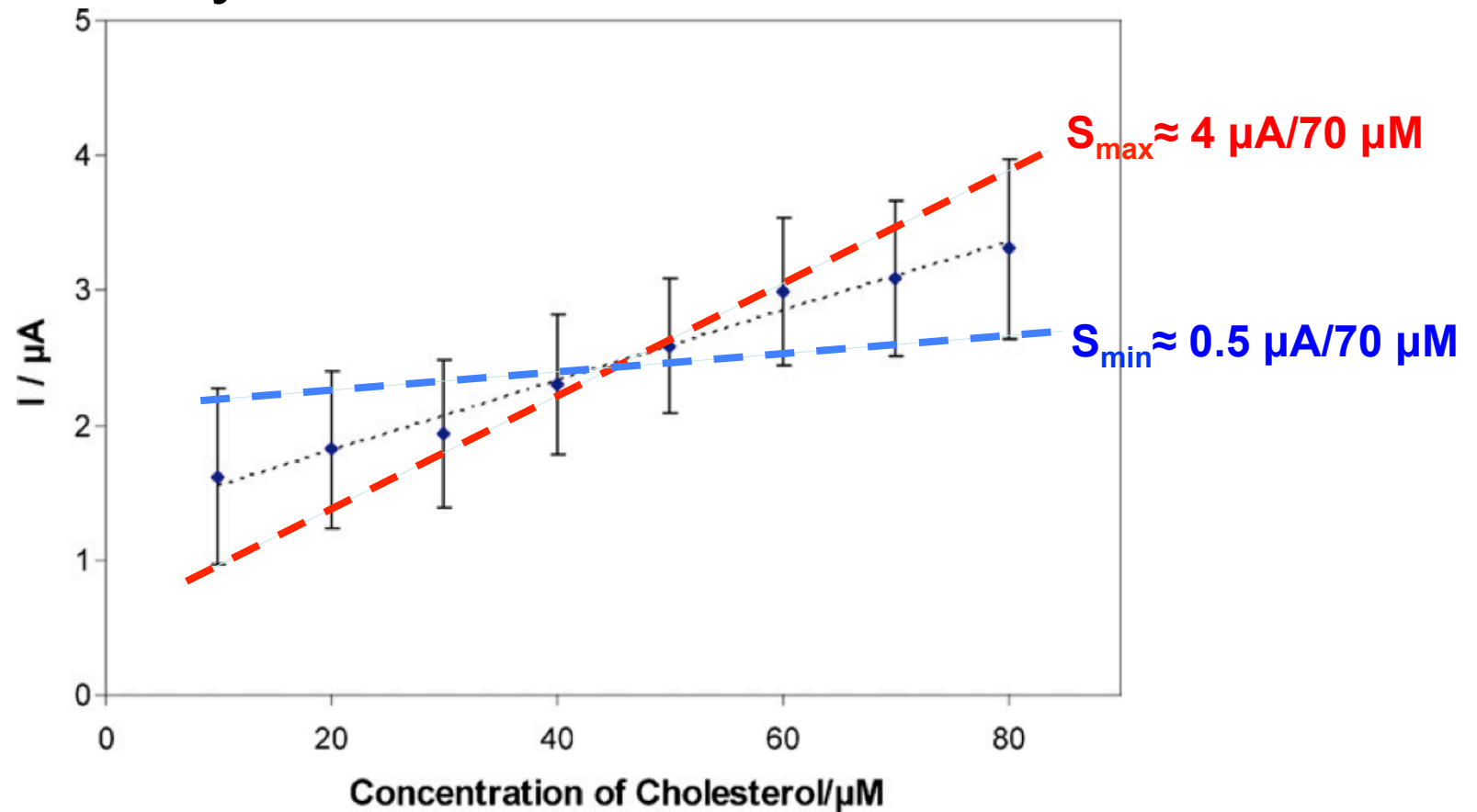
$$S = \frac{\Delta i}{\Delta C} \quad \text{Sensitivity}$$

$$S_A = \frac{S}{A_{WE}} \quad \text{Sensitivity per unit of Area}$$

$$S_A = \frac{\Delta i}{A_{WE} \Delta C} = \frac{nFA_{Active} \sqrt{D}}{A_{WE} \sqrt{\pi t}} \xrightarrow{A_{Active} \rightarrow A_{WE}} \frac{nF \sqrt{D}}{\sqrt{\pi t}}$$

Detection Principle

- Sensitivity: Measurement errors



Detection Principle

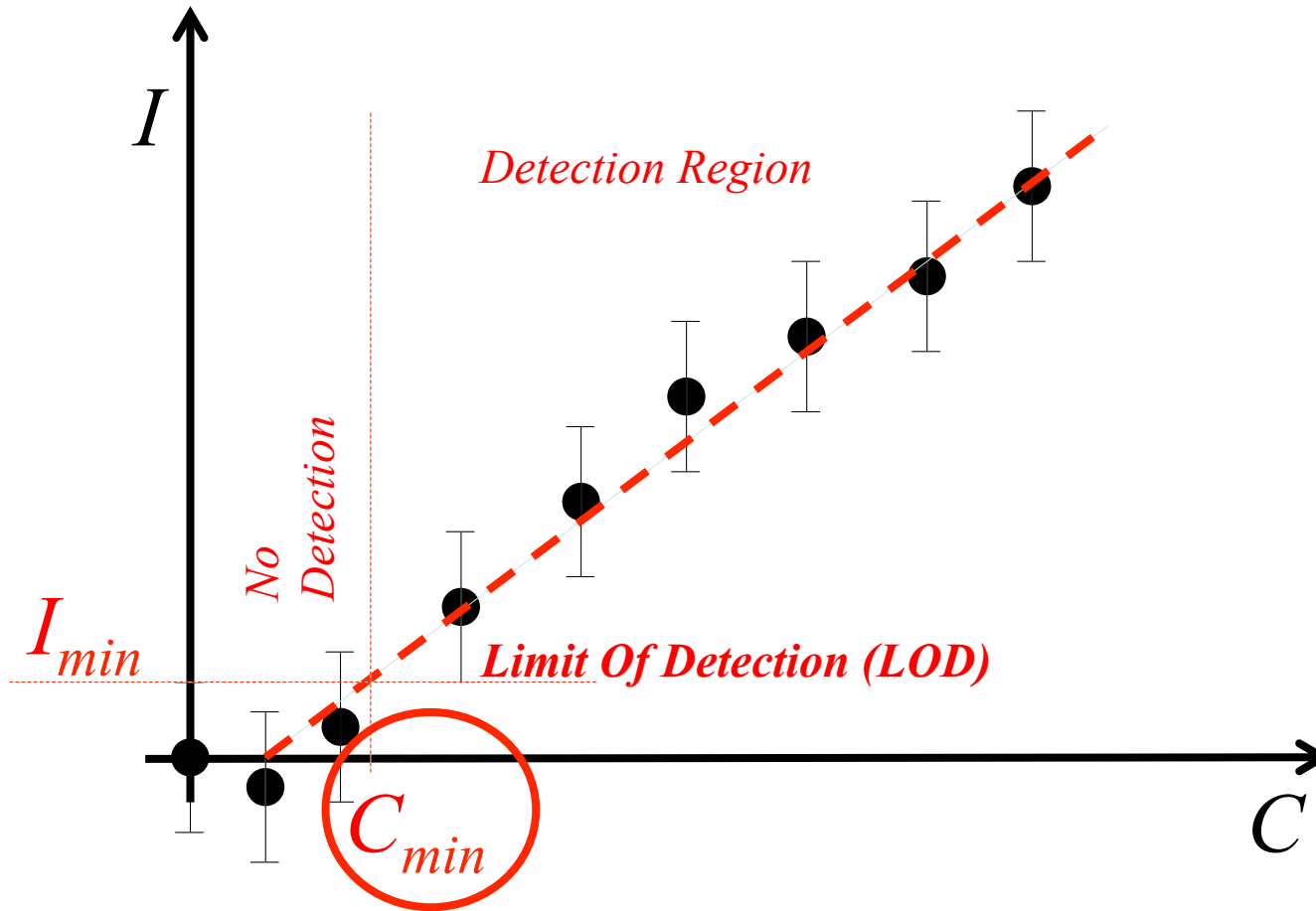
- Sensitivity: Average value and standard its deviation

$$\left. \begin{aligned} S_{\max} &\approx \frac{4 \mu A}{70 \mu M} = 57 \frac{nA}{\mu M} \\ S_{\min} &\approx \frac{0.5 \mu A}{70 \mu M} = 7 \frac{nA}{\mu M} \end{aligned} \right\} \rightarrow \bar{S} = 32 \pm 25 \frac{nA}{\mu M}$$

More correct, because we have measurement errors that do not allow a precise estimation of the sensitivity

Detection Principle

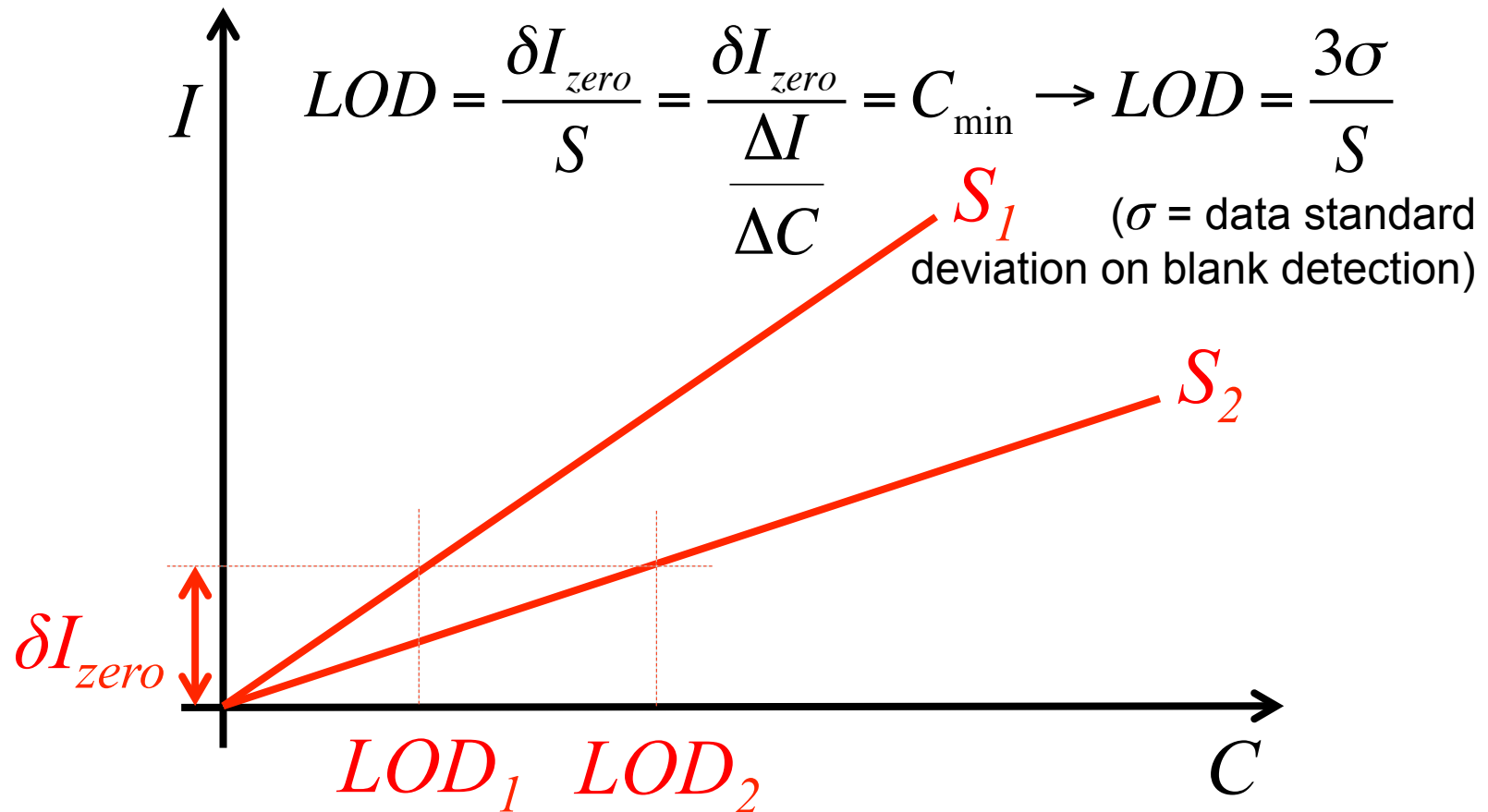
- Detection Limit: a graphic interpretation



(c) S.Carrara

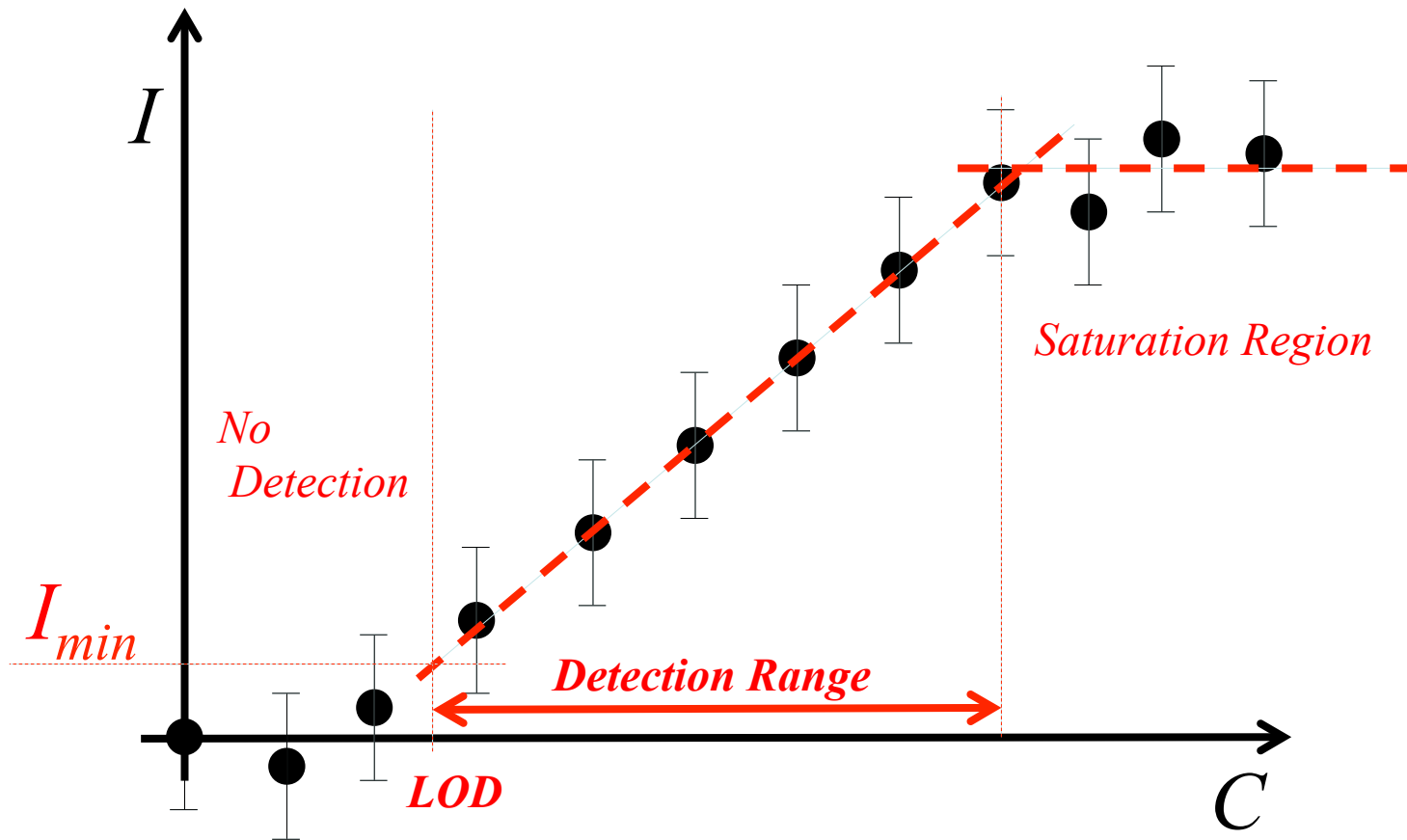
Detection Principle

- Detection Limit: a precise definition



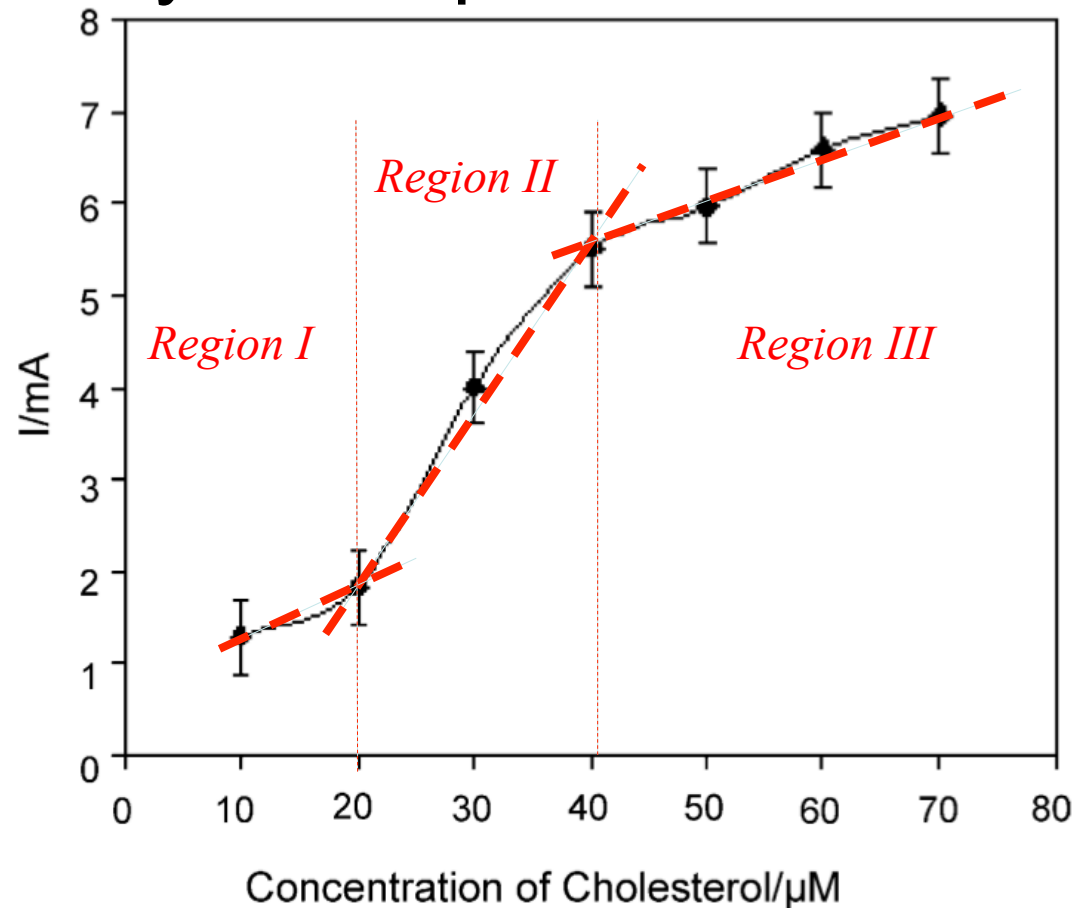
Detection Principle

- Detection Limit: a graphic interpretation



Detection Principle

- Sensitivity: example – A non linear sensor



Sensitivity

- The Clarke's Error Grid

